1	© 2017 Ian M Hodge				
2	CHAPTER TWO: ELECTRICAL RELAXATION				
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Preliminaries

The examples used to illustrate different applications are not central to the purpose of this book and are not recent. Some of the applications have been discussed in an unpublished but widely circulated paper by the present author that is reproduced in Appendix A (original errors have been corrected and the conversion to the phase convention used by everyone except electrical engineers has been made.)

2.1 Nomenclature

- 72 Italicized lower case letters are used for physical variables, e.g. $\{x, y, z, r\}$ for distances, t for
- q time, and q for charge; italicized upper case letters are used for specific values of variables and
- field magnitudes, e.g. {X, Y, Z, R}, T, Q. Vectors are denoted by bold face upper case letters with
- an arrow \mathbf{V} and tensors are denoted by bold face upper case \mathbf{T} .
- 76 There are two time constants for relaxation of polarization, one for relaxation at constant electric
- field (i.e. dielectric relaxation of the displacement $\dot{\mathbf{D}}$) denoted by τ_E and one for relaxation at
- 78 constant displacement (i.e. conductivity relaxation of the electric field $\hat{\mathbf{E}}$) denoted by τ_D .
- Amongst other things these two distinct time constants correspond to two microscopic time
- constants for a single macroscopic dielectric time constant, as has been briefly discussed in ref.

81 [1].

- Dielectric and conductivity relaxations can both occur in the same material over two resolvable frequency ranges and the usual nomenclature for the low and high frequency limits of a single relaxation process (e.g. ε_0 and ε_∞ for the relative permittivity) is ambiguous and has caused confusion in a long standing debate about the legitimacy of the electric modulus formalism. We introduce a new nomenclature here to distinguish the low and high frequency limits for the two possible relaxations that, although somewhat clumsy, eliminates this confusion. The two limits for a dielectric relaxation at constant \mathbf{E} are denoted by ε_0^E and ε_∞^E and the two limits for a conductivity relaxation at constant \mathbf{D} are denoted by ε_0^D and ε_∞^D . Since a conductivity relaxation must in general occur at lower frequencies than a dielectric relaxation for the latter to be readily observed (with some exceptions depending on instrumental sensitivity) then $\varepsilon_\infty^D = \varepsilon_0^E$, although overlap can occur.
- Electric charge is denoted by q (Coulomb C), volume charge density by ρ (C m⁻³), surface charge density by σ C m⁻², linear charge density by λ C m⁻¹, current by I (Ampere = A = C s⁻¹), current density by J (A m⁻²), electric potential by φ_E (V=J C⁻¹), electric field by E (NC⁻¹ = V m⁻¹), electric dipole moment by μ_E (C.m), resistance by R (Ohm = Ω =VA⁻¹), and capacitance by C (Farad F = CV⁻¹). The SI unit for conductance (=1/resistance) is the Siemen S (equal to Ω ⁻¹).

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100 2.2 Electromagnetism

101 2.2.1 Units

Two systems of electromagnetic units are in use, the cgs (centimeter-gram-second) and the MKS (meter-kilogram-second) or SI (Systeme Internationale). The SI system is the official scientific system but the cgs system appears in older publications and since it is still used by chemists and materials scientists its relationship to the SI system is delineated here. For mechanics only the numerical value of physical quantities changes with the system of units, but in electromagnetism there is an additional difference of approach: electric charge in the cgs system is defined in the fundamental units mass-length-time whereas in the SI it is defined to be just as fundamental as mass, length and time: this SI unit of charge is the Coulomb.

The cgs form of Coulomb's law for the force F between two point charges q_1 and q_2 separated by a distance r and immersed in a medium of (dimensionless) permittivity ε is

$$F = \frac{q_1 q_2}{\varepsilon r^2} \,, \tag{2.1}$$

that gives dimensions of $M^{1/2}L^{3/2}T^{-1}$ for the *electrostatic unit* (esu) of charge. The cgs equation for the magnetic force between two straight parallel conductors of length L carrying currents I_1 and I_2 and separated by a distance r in a material of (dimensionless) magnetic permeability μ is

119
$$F = \frac{2\mu L I_1 I_2}{r}$$
, (2.2)

that gives dimensions of $M^{1/2}L^{1/2}$ for the *electromagnetic unit* (emu) of charge. The esu and emu units differ by a factor LT^{-1} that has the dimensions of speed and the value of the speed of light, c. This is the reason that c enters into many cgs formulae. Numerically, emu = c esu (c in cgs units = 2.9979×10^{10} cm/s).

The Coulomb C is defined experimentally by its time derivative, the current in *amperes* A, that in turn is determined using eq. (2.2). A constant μ_0 is inserted into the SI form for this magnetic force to ensure consistency with the cgs system: the same force is produced by the same currents separated by the same distance

130
$$F = \frac{\mu \mu_0 L I_1 I_2}{4\pi r}.$$
 (2.3)

Equations (2.2) and (2.3) reveal that $\mu_0 = 4\pi \times 10^{-7} \text{ N.A}^{-2}$. The factor 4π arises from *Gauss's*

Law [eq. (1.150) and eq. (2.19) below]. The SI form of Coulomb's law is

135
$$F = \frac{q_1 q_2}{4\pi e_0 \varepsilon r^2},$$
 (2.4)

where e_0 is a constant (the *permittivity* of free space), with dimensions $Q^2M^{-1}L^{-3}T^2$ that 137 correspond to the units of capacitance per unit length (Farads meter⁻¹). Comparing eqs. (2.1) and 138 139 (2.4) reveals that

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$$\left(\operatorname{esu}\right)^{2} = \left(\operatorname{Coulomb}\right)^{2} / 4\pi e_{0}. \tag{2.5}$$

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155 156 The numerical relations between C, esu and emu are $C \approx 3 \times 10^9 \text{ esu} \approx 10^{-1} \text{emu}$, where the approximate equality arises from placing the speed of light at 3×10^8 m/s rather than $2.9979...\times10^8$ m/s. The dimensionless fine structure constant α in cgs units is $\alpha = e^2 / hc = 2\pi e^2 / hc$ (e in esu) and in SI units is $\alpha = 2\pi e^2 / 4\pi e_0 hc = e^2 / 2e_0 hc$ (e in Coulomb). It is easily confirmed that the SI value of α is dimensionless and has the same numerical value as the cgs value.

Having illustrated the cgs system to this point it is now dispensed with apart from one exception: the unit for the molecular dipole moment. In the SI system this is the coulomb-meter but this unit is inconveniently large and is rarely (ever?) used. The more common unit is the *Debye*, defined as the dipole moment created by two opposite charges of 10^{-10} esu $(3.3 \times 10^{-20} \text{ C})$ separated by 1.0 Angstrom (10⁻¹⁰ m). The persistence of this unit probably originates in the fact that molecular dipole moments are of order unity when expressed in Debyes but of order 10^{-30} in coulomb-meters. It is not clear to this author why a convenient SI unit such as 10^{-31} C.m ≈ 0.33 Debye or 10^{-30} C.m ≈ 3.3 Debye has not been introduced, especially since the SI unit nm has replaced the Angstrom in optical spectroscopy.

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2.2.2 Electromagnetic Quantities

Many of these are conveniently defined using a parallel plate capacitor comprising two conducting flat plates, each of area A and separated by a distance d. The geometric "cell constant" k is

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$$k \equiv d / A. \tag{2.6}$$

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Each plate has a charge of magnitude q_0 but of opposite sign (uniformly distributed since the plates are conducting) that produces an electric potential difference V between the plates. The capacitance is $C \equiv q_0/V$ that has the units unit Farad = C V⁻¹. The surface charge density $\sigma_0 = \pm q_0 / A$ on the plates induces an interfacial charge density $m\sigma_i$ on each surface of any dielectric material between the plates. The electric field \mathbf{E} , polarization \mathbf{P} and displacement vector $\hat{\mathbf{D}}$ are perpendicular to the plates with magnitudes defined by the following table:

172
173
$$SI \qquad cgs$$
174
$$D = \sigma_0 \qquad D = 4\pi \sigma_0 \qquad (2.7)$$
175
$$P = \sigma_i \qquad P = \sigma_i \qquad (2.8)$$

$$P = \sigma_i \qquad P = \sigma_i \tag{2.8}$$

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176
$$e_0 E = \sigma_0 - \sigma_i = D - P$$
 $E = 4\pi (\sigma_0 - \sigma_i) = D - 4\pi P$ (2.9)

177

The charge densities σ_0 and σ_i generate an electrostatic potential φ_E (in volts) and net volume 178 179 charge density ρ for which

180

$$\mathbf{181} \qquad \mathbf{\dot{D}} = \nabla \rho \tag{2.10}$$

182

183 and

184

$$\mathbf{E} = \nabla \varphi_E. \tag{2.11}$$

186

187 The inverse of eq. (2.11) is

188

189
$$\varphi_{1,2} = \int_{s_1}^{s_2} \mathbf{E} \mathbf{g} d\mathbf{s}$$
 (2.12)

190

where $\varphi_{1,2}$ is the potential difference between the points S_1 and S_2 . The relative permittivity ε 191 and dielectric susceptibility χ_d are defined in the following table:

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204

205

194
$$SI$$
 cgs

195 $\varepsilon = \frac{D}{e_0 E}$ $\varepsilon = \frac{D}{E}$ (2.13)

196
$$\chi_d = \frac{P}{e_0 E} = \frac{D - e_0 E}{e_0 E} = \varepsilon - 1$$
 $\chi_d = \frac{P}{E} = \frac{D - E}{4\pi E} = \frac{1}{4\pi} (\varepsilon - 1)$ (2.14)

A dielectric material between the plates decreases the electric field between the plates because the induced polarization charge density σ_i on the surface of the material partly cancels the unchanged charge density on the plates [eq. (2.9)]. The units of D and P (charge area⁻¹) correspond to dipole moment (charge-distance) per unit volume. In view of $\vec{\mathbf{D}}$, $\vec{\mathbf{E}}$ and $\vec{\mathbf{P}}$ being vectors the relative permittivity and dielectric susceptibility are in general tensors but for isotropic media (liquids, glasses, and isotropic crystals) D, E, P and ε are all scalars. We mostly treat them as scalars in this book.

The magnetic analogs of D, E, P, e_0 , ε and χ_d are, respectively, the magnetic induction B, the magnetic field H, the magnetization M, the permeability of free space, μ_0 , the relative permeability μ , and the magnetic susceptibility χ_m . The SI and cgs definitions are

$$\begin{array}{ccc}
209 & \underline{SI} & \underline{cgs} \\
210 & B = \mu_0 H & B = H
\end{array} \tag{2.15}$$

211
$$M = \frac{B}{\mu_0} - H$$
 $M = \frac{B - H}{4\pi}$ (2.16)

$$212 \qquad \mu = \frac{B}{H} \tag{2.17}$$

213
$$\chi_M = \frac{M}{H} = \frac{B}{\mu_0 H} - 1$$
 $\chi_M = \frac{M}{H} = \frac{B}{4\pi H} - 1$ (2.18)

- 215 2.2.3 Electrostatics
- Gauss's Law is

218
$$\iint_{S} \mathbf{e}_{0} \varepsilon \mathbf{E} \cdot d\mathbf{A} = q_{enclosed} \Rightarrow \iint_{S} \mathbf{D} \cdot d\mathbf{A} = q_{free},$$
 (2.19)

where $q_{\rm enclosed}$ is the total net charge within a closed surface S of magnitude A, ε is the relative permittivity of the material enclosed by the surface, and the surface integral is the flux of the electric field through the surface. For the definition in terms of $\dot{\mathbf{D}}$ the quantity q_{free} does not include the induced polarization charges because these are subsumed into the permittivity $\mathbf{e}_0 \varepsilon$. Equation (2.19) is the electrical version of the mathematical Gauss's Theorem in Chapter One [eq. 1.146)]. As noted in Chapter One the differential area vector $d\mathbf{A}$ of a surface is defined as having a direction perpendicular to the plane of the surface, and for closed surfaces such as occur in Gauss's Law the outward pointing direction is defined to be positive. The Gaussian surface is a purely mathematical object that can be placed anywhere although it must have the same symmetry as the system under study to be helpful. Thus information about charge distribution can be inferred even though E is determined by the *total* enclosed charge.

 Gauss's Law is now used to calculate $\dot{\mathbf{E}}$ and the capacitance C for several geometries and charge distributions. The geometrical objects and charges are taken to be immersed in a medium of relative permittivity ε .

2.2.3.1 Point Charge (Coulomb's Law)

Define the Gaussian surface S as a sphere of radius r with a point charge q at its center. By symmetry \mathbf{E} is everywhere parallel to $d\mathbf{a}$ and has a constant magnitude E obtained from $q = \mathbf{e}_0 \varepsilon \mathbf{\hat{E}} \cdot d\mathbf{A} = 4\pi r^2 \mathbf{e}_0 \varepsilon E$ so that

$$E = \frac{q}{4\pi\varepsilon e_0 r^2} \,. \tag{2.20}$$

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242 2.2.3.2 Long Thin Rod with Uniform Linear Charge Density λ

Define the Gaussian surface to be a cylinder of radius r and length L, with the rod on its central axis. Then $q = \varepsilon e_0 \int_{s}^{L} \cdot d\mathbf{A} = \varepsilon e_0 E(2\pi rL)$ so that at a distance r from the axis

$$246 E = \frac{\lambda}{2\pi\varepsilon e_0 r} \,. (2.21)$$

2.2.3.3 Flat Insulating Plate

Let a charge q be uniformly distributed over the two sides of a flat insulating plate of "infinite area" (no edge effects) so that the charge on each surface is q/2. Define σ as the charge per unit area so that the charge density on each surface is $\sigma/2$. Define the Gaussian surface as a cylinder whose axis is parallel with the area vector of one side of the plate and has one end inside the plate and the other end in a medium of relative permittivity ε . Then the electric field points away from each surface of the plate (since q is positive) and $q/2 = \sigma A/2 = \varepsilon e_0 \sum_{c}^{1} \mathbf{E} \cdot \mathbf{dA} = \varepsilon e_0 EA$

so that

$$E = \frac{\sigma}{2e_0 \varepsilon}. \tag{2.22}$$

This electric field is constant and independent of distance from the plate.

261 2.2.3.4 Flat Conducting Plate

Let the charge on each side of the plate be q/2 and define the Gaussian surface to be the same as that for the insulating plate in §2.2.3.3. The electrostatic field inside a conductor is zero so that the electric field points away each surface of the plate and $q/2 = \sigma A/2 = e_0 \varepsilon \int_{S}^{T} \mathbf{t} \cdot d\mathbf{A} = e_0 \varepsilon EA$ so that

$$E = \frac{\sigma}{2\varepsilon e_0} \,. \tag{2.23}$$

This electric field is again constant and is also independent of distance from the plate

271 2.2.3.5 Two Parallel Insulating Flat Plates

Consider charges $\pm q$ that are uniformly distributed over both surfaces of the plate. The field between the plates is the vector sum of the fields from each plate. Since the field from the positively charged plate points away from the positive plate and the field from the negatively charged plate points toward the negative plate the two fields add up and the electric field is twice that of eq. (2.22):

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$$E = \frac{\sigma}{\varepsilon e_0}.$$
 (2.24)

2.2.3.6 Two Parallel Conducting Flat Plates

Charges $\pm q$ on each plate are attracted to the opposite charges on the other plate so that the charges on each plate will lie totally on the inside surface and the charge density on each interior surface is $\sigma = q/A$. Since the effect of one plate on the other has been taken into account in this case the electric fields do not add up and the field between the plates is again

$$E = \frac{\sigma}{\varepsilon e_0}. \tag{2.25}$$

- The charge density on the outer surface of each plate is zero so that the electric field outside the plates is also zero.
- The capacitance is obtained from the voltage difference $V = E.d\ V$ between the plates and $q = A\sigma_0$:

293
$$C = \frac{q}{V} = \frac{\sigma_0 A}{Ed} = \frac{\sigma_0 A/d}{e_0 \varepsilon / \sigma_0} = (A/d)(e_0 \varepsilon) = (e_0 \varepsilon / k), \qquad (2.26)$$

where k is the "cell constant" corresponding to the effective A/d for the container of the dielectric.

2.2.3.7 Concentric Conducting Cylinders

Define the inner and outer radii of two concentric conducting cylindrical plates to be a and b, respectively, let their equal height be h, and let charges +q and -q be uniformly distributed on the inside surfaces of each plate. Consider a concentric cylindrical Gaussian surface of radius

01
$$a < r < b$$
 and height h , so that $q/e_0 \varepsilon = \int_S \mathbf{E} \cdot d\mathbf{A} = E(2\pi rh)$. Then

$$303 E = q/(2\pi r h e_0 \varepsilon) (2.27)$$

so that

307
$$V = \int_{a}^{b} E dr = \left(\frac{q}{2\pi h e_{0} \varepsilon}\right) \int_{a}^{b} \frac{dr}{r} = \frac{q}{2\pi h e_{0} \varepsilon} \ln\left(\frac{b}{a}\right)$$
 (2.28)

and the capacitance is

311
$$C = \frac{q}{V} = \frac{2\pi h \,\mathrm{e}_0 \varepsilon}{\ln\left(\frac{b}{a}\right)}$$
 (2.29)

- 313 2.2.3.8 Concentric Conducting Spheres
- Define the inner and outer radii of two concentric spherical conducting plates to be a and b, respectively, and let charges +q and -q reside on the inside surfaces of each plate. Consider a
- 316 concentric spherical Gaussian surface of radius a < r < b so that $q/e_0 = \sum_{c}^{1} e^{-c} dA = E[4\pi r^2]$ and
- 317 $E = q/\lceil 4e_0\pi r^2 \rceil$. Then

318

319 $V = \int_{a}^{b} E dr = \frac{q}{4\pi e_{0} \mathcal{E}} \int_{a}^{b} \frac{dr}{r^{2}} = \frac{q}{4\pi e_{0} \mathcal{E}} \left(\frac{1}{b} - \frac{1}{a} \right) = \frac{q}{4\pi e_{0} \mathcal{E}} \left(\frac{a - b}{ab} \right)$ (2.30)

320

- 321 and
- 322 $C = \frac{q}{V} = 4\pi e_0 \varepsilon \left(\frac{ab}{b-a}\right)$. (2.31)

323

- 324 2.2.3.9 Isolated Sphere
- 325 The capacitance of an isolated sphere is obtained from eq. (2.31) by taking the limit
- 326 $b \rightarrow \infty$ and for convenience placing a = R:

327

 $328 C = 4\pi e_0 \varepsilon R. (2.32)$

329

330 Thus larger spheres have larger capacitances.

331

332 2.2.4 Electrodynamics

Consider a constant voltage V applied across two parallel plates between which there is now a conducting medium. Let the resistivity of the material be $\rho = R.k^{-1}$ (units ohm-meter) and specific conductivity $\sigma = 1/\rho$ (units S m⁻¹), where R is the resistance between the plates in ohms and the symbol S refers to the SI unit Siemen defined as the reciprocal of the ohm. The current density \mathbf{J} is the electric current per unit area (units A m⁻²) so that $\mathbf{J}\rho = \mathbf{E}$. Unfortunately the displacement current $dD/dt = d\sigma_0/dt$ (better named as the displacement current density) has no

339 symbol.

Electric current, symbol *I*, is defined as

340341

 $342 I = \frac{dq}{dt} (2.33)$

343

so that the total charge that passes across a plane through which a current *I* flows is

345

 $346 q = \int_{0}^{t} I \, dt'. (2.34)$

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348 The electric potential φ_E is not defined for electrodynamics (see §2.5 below on Maxwell's

349 equations) and is replaced by the symbol voltage V (unfortunately also used for the unit volt).

350 Ohm's Law for the electrical resistance R (SI unit ohm (Ω) is then

351

$$R \equiv \frac{V}{I} \tag{2.35}$$

353

354 and $\Omega = V/A$. An electrical conductor is said to be ohmic if, and only if, R is constant. This is not the same as dV/dI = constant: for example if V = 1.0 + 2I so that dV/dI = 2 then 355

356
$$R = 3\Omega$$
 for $I = 1A$, $R = 2.5\Omega$ for $I = 2A$, $R = 2.3\Omega$ for $I = 3A$.

Resistances dissipate power P given by P = IV (recall that energy is given by QV and power is the time derivative of energy). For ohmic resistances

358 359

357

$$P = IV$$

360 =
$$I(IR) = I^2R$$
 (2.36)
= $(V/R)V = V^2/R$.

361 362

363

364

365

2.2.5 Maxwell's Equations

These four equations summarize all that is known about electromagnetic phenomena – they are essentially the electromagnetic equivalent of Newton's laws for mechanics but more mathematically sophisticated because of the greater complexity of electromagnetic phenomena.

The differential forms of the four Maxwell equations are:

366 367

368
$$\nabla g \mathbf{D} = \rho;$$
 (2.37)

$$\begin{array}{ccc}
369 & \sqrt[3]{\mathbf{g}} \mathbf{B} = 0;
\end{array} \tag{2.38}$$

368
$$\nabla \mathbf{g} \mathbf{D} = \rho;$$
369
$$\nabla \mathbf{g} \mathbf{B} = 0;$$
370
$$\nabla \times \mathbf{E} = -\left(\frac{\partial \mathbf{B}}{\partial t}\right);$$
(2.37)
(2.38)

371
$$\overset{\mathbf{r}}{\nabla} \times \overset{\mathbf{r}}{\mathbf{H}} = \overset{\mathbf{r}}{\mathbf{J}} + \left(\frac{\partial \overset{\mathbf{b}}{\mathbf{D}}}{\partial t} \right)$$
 (2.40)

$$= \sigma \mathbf{E}^{\mathbf{r}} + \left(\frac{\partial \mathbf{D}}{\partial t}\right) \tag{2.41}$$

373
$$= \sigma \mathbf{E}^{\mathbf{r}} + \mathbf{e}_0 \left(\frac{\partial \varepsilon \mathbf{E}}{\partial t} \right). \tag{2.42}$$

374

375 Equation (2.40) for a vacuum is equivalent to

377
$$\nabla \times \mathbf{B} = \mu_0 \mathbf{J} + \mu_0 \mathbf{e}_0 \left(\frac{\partial \mathbf{E}}{\partial t} \right), \tag{2.43}$$

where σ is the specific electrical conductivity (units $(\Omega^{-1} m^{-1} = S m^{-1})$, \mathbf{B} is the magnetic induction, and \mathbf{H} is the magnetic field. Equations (2.40) - (2.42) merit some discussion. The equation $\nabla \times \mathbf{H} = \mathbf{J}$ might perhaps be expected instead of eq. (2.40) but this has the nonsensical implication that there could never be any sources or sinks of current anywhere at any time, because the vector identity $\nabla g (\nabla \times \mathbf{H}) = 0$ would then imply $\nabla g \mathbf{J} = 0$. The difficulty is resolved by noting that for a charging or discharging parallel plate capacitor (for example) charge flow in the external circuit joining the two capacitor plates, corresponding to dq_0/dt where q_0 is the charge on the capacitor plates (see §2.1.2 above), must be compensated for by an opposite change of the polarization charges between the plates (to ensure charge conservation). Thus

$$\overset{\mathbf{r}}{\nabla} \mathbf{g} \left(\overset{\mathbf{r}}{\nabla} \times \overset{\mathbf{r}}{\mathbf{H}} \right) = 0 = \overset{\mathbf{r}}{\nabla} \left[\left(\frac{\partial q_0}{\partial t} \right) - \left(\frac{\partial q_i}{\partial t} \right) \right]$$
(2.44)

is ensured.

The term $\partial \mathbf{D}/\partial t$ in eq. (2.40) can correspond for example to a localized (molecular diameter) effective spatial translation of charge due to rotation of an electric dipole about its center of mass that has a close analogy to an ion hopping to an adjacent site (see §2.2.1.2). It is called the *displacement current*. The term displacement "current" has been claimed to be a misnomer but this is true only if a current is interpreted to be a long range translational migration of charge. If the definition of current as dq/dt is adopted it is not a misnomer because q (on capacitor plates for example) changes with time [eq. (2.44)], and furthermore a traditional current must be present in an external circuit to compensate for $\partial q_i/\partial t$. Describing $\partial \mathbf{D}/\partial t$ as a "fictitious current", as has been done in at least one popular text book, is disingenuous and misleading because eq. (2.40) demonstrates that $\partial \mathbf{D}/\partial t$ is just as important in determining a magnetic field as migration of individual charges.

The vector potential $\hat{\mathbf{A}}$ is defined by

$$403 \qquad \stackrel{\mathbf{1}}{\nabla} \times \mathbf{A} = \mathbf{B} \tag{2.45}$$

405 and

$$407 \qquad \mathbf{E} = -\nabla \varphi_E - \frac{\partial \mathbf{A}}{\partial t}, \qquad (2.46)$$

and essentially ensures consistency between electrostatics and electrodynamics. Equation (2.45) ensures eq. (2.38) because of the vector identity $\nabla g (\nabla \times \mathbf{A}) = 0$ and eqs. (2.45) and (2.46) together ensure that eq. (2.39) remains true in dynamic situations where φ_E is undefined. The vector potential is essentially an extension of the Coulomb potential φ_E to dynamic situations because the definition of φ_E from $\mathbf{E} = \nabla \varphi_E$ [eq. (2.11)] is definable only in static situations, as the

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following consideration indicates: if $\partial \mathbf{B} / \partial t \neq 0$ then $\nabla \times \mathbf{E} \neq 0$ by eq. (2.38) and the static

415 relation

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440

444

$$\begin{array}{ccc}
416 \\
417 & \mathbf{E} = \nabla \varphi_E
\end{array} \tag{2.47}$$

could then never hold because of the vector identity $\overset{\mathbf{r}}{\nabla} \times (\overset{\mathbf{r}}{\nabla} \varphi_{E}) = 0$. But $\overset{\mathbf{r}}{\mathbf{E}}$ is known to be

- nonzero in dynamic situations [CHECK]. Similarly if $\mathbf{J} \neq 0$ or $\partial \mathbf{D} / \partial t \neq 0$ then there is no
- potential φ_B for \mathbf{B} (defined by $\mathbf{B} = \nabla \varphi_B$) because eq. (2.40) then implies $\nabla \times \mathbf{H} = \nabla \times \mathbf{B} / \mu \mu_0 \neq 0$
- because of the same vector identity $\overset{\mathbf{r}}{\nabla} \times (\overset{\mathbf{r}}{\nabla} \varphi_B) = 0$. Both these difficulties are averted by the
- introduction of $\hat{\mathbf{A}}$. Equation (2.46) is then consistent with eq. (2.39) since it guarantees

425
$$\overset{\mathbf{r}}{\nabla} \times \overset{\mathbf{r}}{\mathbf{E}} = \overset{\mathbf{r}}{\nabla} \times \left(-\overset{\mathbf{r}}{\nabla} \varphi_E - \frac{\partial \overset{\mathbf{r}}{\mathbf{A}}}{\partial t} \right) = -\frac{\partial \overset{\mathbf{r}}{\mathbf{B}}}{\partial t}.$$
 (2.48)

427 Integral versions of Maxwell's equations include Faraday's Law:

429
$$\int_{\mathbf{E}}^{\mathbf{r}} \mathbf{g} d\mathbf{s} = -\frac{d\Phi_{B}}{dt}; \qquad \Phi_{B} \equiv \int_{\mathbf{R}}^{\mathbf{r}} \mathbf{g} d\mathbf{A} = \text{magnetic flux}$$
 (2.49)

and Ampere's law

433
$$\mathbf{\tilde{N}}_{E}^{\mathbf{r}} \mathbf{g} d\mathbf{\tilde{s}} = \mu_{0} \mathbf{e}_{0} \frac{d\Phi_{E}}{dt} + \mu_{0} I_{enclosed}; \quad \Phi_{E} \equiv \mathbf{\tilde{N}}_{E}^{\mathbf{r}} \mathbf{g} d\mathbf{\tilde{A}} = \text{electric flux}.$$
 (2.50)

Equation (2.42) provides a convenient demonstration of the equivalence of the complex permittivity and complex conductivity. First convert eq. (2.42) from a vector equation to a complex scalar equation:

439
$$\nabla \times \mathbf{H} = \sigma \mathbf{E} + \mathbf{e}_0 \left(\frac{\partial \varepsilon \mathbf{E}}{\partial t} \right) \Rightarrow |\nabla \times \mathbf{H}| = \sigma * E * + \mathbf{e}_0 \varepsilon * \left(\frac{\partial E *}{\partial t} \right).$$
 (2.51)

441 For a sinusoidal excitation $E^* = E_0 \exp(-i\omega t)$ eq. (2.51) becomes

442
$$\begin{vmatrix}
\nabla \times \mathbf{H} \\
\nabla \times \mathbf{H}
\end{vmatrix} = \sigma^* E_0 \exp(-i\omega t) - e_0 \varepsilon^* E_0(i\omega) \exp(-i\omega t)$$
443
$$= \left[\sigma^* - i\omega e_0 \varepsilon^*\right] E_0 \exp(-i\omega t)$$

$$= \left[\varepsilon^* - \sigma^* / (i\omega e_0)\right] (-ie_0 \omega) E_0 \exp(-i\omega t),$$
(2.52)

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indicating that both the complex conductivity $\left[\sigma^*-i\omega e_0\varepsilon^*\right]$ and complex permittivity $\left[\varepsilon^*-\sigma^*/(i\omega e_0)\right]$ provide equivalent descriptions of electrical relaxation, as do the resistivity $\rho^*=1/\sigma^*$ and electric modulus $M^*=1/\varepsilon^*$. All these different functions emphasize or suppress different facets of experimental data in the same way that Fourier transforms do for example [see eq. (2.106) below].

451 2.2.6 Electromagnetic Waves

The Maxwell equations together with the constitutive relations $\mathbf{D} = \mathbf{e}_0 \varepsilon \mathbf{E}$ and $\mathbf{B} = \mu_0 \mu \mathbf{H}$ 453 predict transverse electromagnetic (em) waves traveling at the speed of light c/n given by

455
$$\frac{c}{n} = \frac{\left(1/e_0 \mu_0\right)^{1/2}}{\left(\varepsilon \mu\right)^{1/2}} = \frac{1}{\left(e_0 \varepsilon \mu_0 \mu\right)^{1/2}},$$
 (2.53)

457 where

$$459 n = \left(\varepsilon\mu\right)^{1/2} (2.54)$$

461 is the refractive index. In a nonmagnetic material for which $\mu = 1$ and $\varepsilon^* = (n^*)^2$

463
$$(n^*)^2 = (n'-in'')^2 = (n'^2-n''^2)-2in'n'' = \varepsilon^* = \varepsilon'-i\varepsilon''$$
 (2.55)

465 so that

467
$$\varepsilon' = n'^2 - n''^2$$
 (2.56)

469 and

$$\varepsilon'' = 2n'n''. \tag{2.57}$$

For the general case of a magnetic material where the relative magnetic permeability is also complex, $\mu^* = \mu' - i\mu''$,

476
$$(n^*)^2 = (n'^2 - n''^2) - 2in'n'' = (\varepsilon' - i\varepsilon'')(\mu' - i\mu'')$$
 (2.58)

478 so that

$$480 \qquad \left(n^*\right)^2 = \left(n'^2 - n''^2\right) - 2in'n'' = \left(\varepsilon' - i\varepsilon''\right)\left(\mu' - i\mu''\right) = \left(\varepsilon'\mu' - \varepsilon''\mu''\right) - i\left(\varepsilon'\mu'' + \varepsilon''\mu''\right), \tag{2.59}$$

482 and

$$484 n'' = (\varepsilon' \mu'' + \varepsilon'' \mu'). (2.60)$$

Thus absorption of electromagnetic energy by magnetically lossy materials is enhanced by a high relative permittivity and dielectric loss is enhanced in magnetic materials.

The electric field component of a plane electromagnetic traveling wave of angular frequency ω propagating in the +x direction in a medium with refractive index n and speed c/n is

$$490 E(x,t) = E_0 \exp\left\{-i\omega\left[t - \frac{nx}{c}\right]\right\}, (2.61)$$

and similarly for the magnetic field component. For complex $n^* = n' - in''$ eq. (2.61) becomes

$$E(x,t) = E_0 \exp\left\{-i\omega \left[t - \frac{(n'-n'')x}{c}\right]\right\}$$

$$= E_0 \exp\left\{-i\omega \left[t - \frac{n'x}{c}\right]\right\} \exp\left[\frac{-n''\omega x}{c}\right],$$
(2.62)

so that E decays exponentially with distance +x into the medium. The intensity $I = |E|^2$ of em waves is then

$$I = E_0^2 \exp\left\{-2i\omega \left[t - \frac{(n' - in'')x}{c}\right]\right\}$$

$$= E_0 \exp\left\{-2i\omega \left[t - \frac{n'x}{c}\right]\right\} \exp\left[\frac{-2n''\omega x}{c}\right],$$
(2.63)

that is to be compared with Beer's Law

$$I = I_0 \exp(-\alpha x), \tag{2.64}$$

where α is the extinction coefficient (usually expressed in neper m⁻¹ where the dimensionless neper is used to emphasize that the logarithmic form of eq. (2.64) implies the Naperian logarithm). Equations (2.63) and (2.64) yield

509
$$\alpha(\omega) = \frac{2\omega n''(\omega)}{c}$$
. (2.65)

The sign convention for imaginary numbers mentioned in the Introduction of Chapter One seen at work here. If the sinusoidal perturbation was defined as

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 $E(x,t) = E_0 \exp\{+i\omega[t-nx/c]\}$ and the sign of the imaginary component of ε^* remained negative then α would have to be negative and Beer's Law would predict unphysical exponential growth through a medium. This can be resolved by making the imaginary component of ε^* positive but this corresponds to a dipole rotation that leads the excitation voltage rather than lags it. Nonetheless this is the convention used by electrical engineers and is the price paid for the "advantage" of having a positive sign in the complex exponential. An excellent account of phase conventions is given in Chapter One of ref. [2].

Insertion of eq. (2.57) into eq. (2.65) yields

522
$$\alpha(\omega) = \frac{\omega \varepsilon''(\omega)}{n'(\omega)c}$$
, (2.66)

524 and since $\varepsilon'' = \sigma'/(e_0 \omega)$ then

526
$$\alpha(\omega) = \frac{\sigma'(\omega)}{n'(\omega)e_0c}$$
. (2.67)

Thus $n'', \varepsilon'', \alpha$ and σ' are all measures of absorption of electrical energy:

530
$$\alpha = \frac{\sigma'}{ne_0c} = \frac{\omega\varepsilon''}{nc} = \frac{2\omega n''}{c}$$
 (2.68)

Ordinary em radiation comprises randomly distributed directions of polarization for the $\stackrel{1}{\mathbf{E}}$ and $\stackrel{1}{\mathbf{B}}$ fields (that are always perpendicular to one another). Radiation for which the direction of polarization is constant and the same for all waves is said to be polarized. Reflected em waves are partially polarized in the direction parallel to the reflecting surface, the extent of polarization depending on the angle of incidence. Polaroid® sun glasses are polarized in the vertical direction and therefore more strongly attenuate reflected waves. Reflected em waves are fully polarized at the Brewster incident angle.

2.2.7 Local Electric Fields

The electric field inside a dielectric medium is not equal to the applied field because of electrostatic screening by the medium. This is a complicated problem that is well described in Chapter One of ref. [3] (by N. E. Hill) and has been considered by Onsager [4], Kirkwood [5], and Frohlich [6]. The complexity of the issue is illustrated by the Kirkwood relation between the isolated molecular dipole moment μ_g observed in the gas phase and the relative permittivity ε_0^E

$$547 \qquad \frac{4\pi Ng \,\mu_g^2}{9k_B T V \mathbf{e}_0} = \frac{\left(\varepsilon_0^E - \varepsilon_\infty^E\right) \left(2\varepsilon_0^E + \varepsilon_\infty^E\right)}{\varepsilon_0^E \left(\varepsilon_\infty^E + 2\right)},\tag{2.69}$$

where ε_{∞}^{E} is the limiting high frequency relative permittivity that for a pure dielectric equals the square of the (limiting low frequency) refractive index n^{2} , N is the number of dipoles in a volume V, and g is a correlation factor that corrects for nonrandom orientations of surrounding dipoles caused by direction dependent intermolecular forces. The latter is in principle calculable:

554
$$g = 1 + \sum_{i \neq j}^{N} \left\langle \cos\left(\theta_{ij}\right) \right\rangle,$$
 (2.70)

where the averaged cosine $\langle \cos(\theta_{ij}) \rangle$ of the angle θ_{ij} between dipoles μ_i and μ_j can be computed for specific orientation geometries.

The treatment of local field effects on the kinetics of dipole relaxation is even more intricate because the reaction field produced by polarization of the dielectric medium by the embedded dipole is in general out of phase with the applied field. These effects have been discussed by Mountain [7]. A particularly important effect of local fields on relaxation phenomenology is that a single macroscopic dielectric relaxation time corresponds to two microscopic times. After a heated debate in the literature the accepted microscopic dipole correlation function is the Fatuzzo and Mason [8] expression

$$\varphi(t) = \left(1 + \frac{\varepsilon_{\infty}}{2\varepsilon_{0}}\right)^{-1} \left[\exp\left(-\frac{t}{\tau_{E}}\right) + \left(\frac{\varepsilon_{\infty}}{2\varepsilon_{0}}\right) \exp\left(-\frac{\varepsilon_{0}}{\varepsilon_{\infty}} \frac{t}{\tau_{E}}\right)\right]$$

$$= \left(1 + \frac{\varepsilon_{\infty}}{2\varepsilon_{0}}\right)^{-1} \left[\exp\left(-\frac{t}{\tau_{E}}\right) + \left(\frac{\varepsilon_{\infty}}{2\varepsilon_{0}}\right) \exp\left(-\frac{t}{\tau_{D}}\right)\right],$$
(2.71)

where τ_E and τ_D are again the relaxation times for polarization at constant E and D respectively. Fulton [9] has given a detailed discussion of this subject in which he deduced that the longitudinal part of polarization relaxes with a time constant τ_D and that the transverse component relaxes with a time constant τ_E . Electrical relaxation is therefore discussed later in this chapter in two parts - dielectric relaxation and conductivity relaxation.

2.2.8 Circuits

There are the four fundamental elements in analog passive circuits: resistance R; capacitance C; self inductance L; mutual inductance M.

2.2.8.1 Simple Circuits

Resistances in Series and in Parallel

For resistances R_i connected in series the same current I must pass through each and the sum of the voltages across each resistor equals the applied voltage. Thus $V = \sum V_i = I \sum R_i = IR_s$ and the equivalent series resistance R_s is

$$584 R_s = \sum_i R_i . (2.72)$$

For resistances R_i connected in parallel the same voltage V must occur across each and the total current I through the parallel circuit is the sum of the currents through each resistance: $I = \sum I_i = \sum V / R_i$ so that the equivalent parallel resistance R_p is given by

$$590 1/R_p = \sum 1/R_i. (2.73)$$

Capacitances in Series and in Parallel

Capacitance C is defined as C = q/V, where V is the voltage across the capacitor and $\pm q$ are the charges on each of its ends. For capacitances C_i connected in parallel the same voltage V must occur across each and the total charge q on each side of the equivalent parallel capacitance C_p must equal the sum of charges q_i on each component. Thus

 $q = \sum_{i} q_i = V \sum_{i} C_i = C_p V$ and the equivalent parallel capacitance C_p is given by

$$599 C_p = \sum_{i} C_i . (2.74)$$

For capacitances connected in series the total voltage V across the series circuit equals the sum of voltages across each capacitor. The magnitude of the charges q on each must be the same (since no charge separation can occur across the short circuit joining them) so that $V = q/C_s = \sum_i V_i = \sum_i q/C_i$ and the equivalent series capacitance C_s is given by

606
$$\frac{1}{C_s} = \sum_{i} \frac{1}{C_i}.$$
 (2.75)

608 Inductances in Series and in Parallel

The self-inductance L is defined as $L \equiv V / (dI / dt)$ where V is the voltage across the device and I is the current through it. Since V is in the numerator and I is in the denominator L is an impedance akin to R. Impedances add in series so the equivalent series inductance L_s is

613
$$L_s = \sum_i L_i$$
, (2.76)

and since admittances add in parallel the equivalent parallel inductance I_p is

617
$$\frac{1}{L_s} = \sum_{i} \frac{1}{L_i}$$
 (2.77)

For the sake of completion the mutual inductance M is now described although for reasons given below it rarely comes into play for relaxation phenomena or insrumentation. It is defined as $M = V_2/(dI_1/dt)$, where V_2 is the voltage induced on one side of the device by a time varying current I_1 in the other. Rearrangement of this definition of M yields

624
$$V_2 = M(dI_1/dt),$$
 (2.78)

so that V_2 is smaller at lower frequencies when dI_1/dt is smaller. This is why transformer arm (ac Wheatstone) bridges are useless at low frequencies. Series and parallel combinations of mutual inductances add up in the same way as self inductances.

630 Combined Series and Parallel Elements

Consider two examples of a circuit in which an element Z_1 is in parallel with a series combination of two elements Z_2 and Z_3 . If these elements are resistances R_1 , R_2 and R_3 then $R_{23} = R_2 + R_3$ and

635
$$\frac{1}{R_{equiv}} = \frac{1}{R_1} + \frac{1}{R_2 + R_3} = \frac{R_1 + R_2 + R_3}{R_1 (R_2 + R_3)}$$
 (2.79)

637 or

639
$$R_{equiv} = \frac{R_1(R_2 + R_3)}{R_1 + R_2 + R_3}$$
 (2.80)

If these elements are capacitances C_1 , C_2 and C_3 then $642 \quad 1/C_{23} = 1/C_2 + 1/C_3 \Rightarrow C_{23} = C_2C_3/(C_2 + C_3)$ and

644
$$C_{equiv} = C_1 + C_{23} = C_1 + \frac{C_2 C_3}{C_2 + C_3} = \frac{C_1 C_2 + C_2 C_3 + C_3 C_1}{C_2 + C_3}$$
 (2.81)

646 2.2.8.2 AC Circuits

If a voltage $V(t) = V_0 \cos(\omega t) = \text{Re}[V_0 \exp(-i\omega t)]$ is applied across a circuit the average voltage over one period is zero but the ac power is not. Equation (2.36) indicates that power is determined by the averages of I^2 and V^2 that are both proportional to the averages of $\sin^2(\omega t)$ or $\cos^2(\omega t)$ over one cycle that are both equal to $\frac{1}{2}$. Thus

652
$$P_{average} = (V_0^2 / 2)R = I_0^2 R / 2.$$
 (2.82)

The ac power dissipation is therefore given by the same relation for DC power dissipation if the

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- maximum ac voltage (V_0) and current (I_0) are replaced by $V_0/2^{1/2}$ and $I_0/2^{1/2}$ respectively. The latter are referred to as rms (root mean square) voltages and currents. Electrical outlet ac voltages
- such as 120V in North America are given as rms values; the peak voltage in North America is
- therefore $(120V)(2)^{1/2} = 170V$.
- AC impedances $Z^*(i\omega)$ are defined as $V^*(i\omega)/I^*(i\omega)$ and ac admittances $A^*(i\omega)$ as
- $I^*(i\omega)/V^*(i\omega)$. The imaginary components of $A^*(i\omega)$ and $Z^*(i\omega)$ are referred to as
- reactances, and as shown below do not dissipate power.
- Resistances
- For a voltage $V = V_0 \exp(-i\omega t)$ applied across a resistance R the current is

666
$$I_{R}(i\omega t) = \frac{V(i\omega t)}{R} = \frac{V_{0}}{R} \exp(-i\omega t) = V_{0}G \exp(-i\omega t)$$
(2.83)

- so that the impedance is

670
$$Z_{R}^{*}(i\omega t) = \frac{V * (i\omega t)}{I * (i\omega t)} = \frac{V_{0} \exp(-i\omega t)}{(V_{0} / R) \exp(-i\omega t)} = R$$
 (2.84)

- and the admittance $A_R^*(i\omega t) = 1/Z_R^*(i\omega t) = G$ where G is the conductance. Both R and G are real
- and independent of frequency.
- **Capacitances**
- For a capacitance C the current is

678
$$I_{C}(i\omega t) = \frac{dq(\omega t)}{dt} = C\frac{dV(i\omega t)}{dt} = V_{0}[-i\omega C \exp(-i\omega t)], \qquad (2.85)$$

- the capacitive impedance is

682
$$Z_C^*(i\omega t) = \frac{V^*(i\omega t)}{I_C^*(i\omega t)} = \frac{V_0 \exp(-i\omega t)}{V_0 \left[-i\omega \exp(-i\omega t)\right]} = \frac{1}{-i\omega C} = \frac{i}{\omega C},$$
 (2.86)

- the capacitive admittance is

$$A_C^*(i\omega t) = -i\omega C. \tag{2.87}$$

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687

The capacitive admittance and admittance are therefore frequency dependent and imaginary.

Power dissipation per cycle in a capacitance is given by

690

$$P_{C}(t) = \langle V_{C}(t) I_{C}(t) \rangle = \langle \left[V_{0} \exp(-i\omega t) \right] V_{0} \left[-i\omega C_{p} \exp(-i\omega t) \right] \rangle = -V_{0}^{2} \omega C_{p} \langle \exp(-2i\omega t) \rangle$$

$$= \langle -V_{0}^{2} \omega C_{p} \left[\cos(-2\omega t) - i\sin(-2\omega t) \right] \rangle$$

$$= \langle -V_{0}^{2} \omega C_{p} \left[\cos(2\omega t) + i\sin(2\omega t) \right] \rangle$$

$$= 0$$

$$(2.88)$$

692

because the averages of both $\cos(2\omega t)$ and $\sin(2\omega t)$ over one cycle are zero. The capacitive

694 impedance is therefore not a resistance if "resistance" is taken to imply power dissipation. This is

why an inductive or capacitive impedance is not considered to be an "ac resistance".

696

697 Inductances

For a self-inductance L the current is

698 699

700
$$I_{L}(\omega t) = \int \left(\frac{V}{L}\right) dt = \int \left(\frac{V_{0} \exp(-i\omega t)}{L}\right) dt = \left(\frac{V_{0}}{L}\right) \frac{\exp(-i\omega t)}{-i\omega}$$
 (2.89)

701 702

so that inductive impedance is

703

$$Z_L^*(i\omega t) = \frac{V^*(i\omega t)}{I_L^*(i\omega t)} = -i\omega L$$
 (2.90)

705 706

and the inductive admittance is

707

$$708 A_L^*(i\omega t) = \frac{1}{-i\omega L} = \frac{i}{\omega L}. (2.91)$$

709 710

The inductive reactance is therefore also imaginary and frequency dependent. Power dissipation

in an inductance is given by

711 712

713
$$P_{L}(t) = \langle V_{L}(t) I_{L}(t) \rangle = \left\langle \left[V_{0} \exp(-i\omega t) \right] \left(\frac{V_{0}}{L} \right) \frac{\exp(-i\omega t)}{-i\omega} \right\rangle$$

$$= -\frac{V_{0}^{2}}{-i\omega L} \left\langle \exp(-2i\omega t) \right\rangle = \frac{V_{0}^{2}}{i\omega L} \left\langle \exp(-2i\omega t) \right\rangle = 0.$$
(2.92)

714

715 Thus the power dissipated by a pure inductance is zero just like that of a capacitance ("pure"

716 meaning negligible resistance).

718 Parallel Resistance and Capacitance

Consider a voltage $V = V_0 \cos(\omega t)$ applied across a resistance R_p in parallel with a capacitance C_p . The current I_R through the resistance is

721

722
$$I_{R} = \frac{V}{R_{p}} = \frac{V_{0}\cos(\omega t)}{R_{p}} = V_{0}\cos(\omega t)G_{p} = \text{Re}\left[V_{0}G_{p}\exp(-i\omega t)\right]$$
 (2.93)

723 724

where $G_p = 1/R_p$ is the conductance. The current through the capacitance I_C is

725

726
$$I_{C} = \frac{dq_{C}}{dt} = C_{p} \frac{dV}{dt} = -V_{0}\omega C_{p} \sin(\omega t)$$

$$= -V_{0}\omega C_{p} \cos(\omega t - \pi/2) \operatorname{Re}\left[-iV_{0}\omega C_{p} \exp(-i\omega t)\right]$$
(2.94)

727

- where q_C is the charge on the capacitor. Equation (2.94) implies that the sinusoidal (displacement)
- 729 current I_C lags the applied voltage by $\pi/2$ radians because $\sin(\omega t) = \cos(\omega t \pi/2)$. The total
- 730 current through the parallel R_pC_p circuit is

731

$$I = I_{R} + I_{C} = V_{0}G_{p}\cos(\omega t) - V_{0}\omega C_{p}\sin(\omega t)$$

$$= \operatorname{Re}\left[V_{0}G_{p}\exp(-i\omega t)\right] + \operatorname{Re}\left[-iV_{0}\omega C_{p}\exp(-i\omega t)\right]$$

$$= \operatorname{Re}\left\{V_{0}\left[G_{p} - i\omega C_{p}\right]\exp(-i\omega t)\right\}.$$
(2.95)

733

The phase relations for the current are therefore conveniently expressed by defining the parallel combination of resistance and capacitance as a complex admittance A^*

736

737
$$A^* = G_p - i\omega C_p, \qquad (2.96)$$

738

739 or as a complex impedance Z^*

740

741
$$Z^* = 1/A^* = \frac{1}{G_p - i\omega C_p} = \frac{G_p}{G_p^2 + \omega^2 C_p^2} + \frac{i\omega C_p}{G_p^2 + \omega^2 C_p^2}$$
 (2.97)

742

743 The complex capacitance is

744

745
$$C^* = \frac{A^*}{-i\omega} = C_p + \frac{iG_p}{\omega}$$
 (2.98)

746

and the complex electric modulus is

749
$$M*(i\omega) = 1/C*(i\omega) = i\omega Z*(i\omega). \tag{2.99}$$

751 Equation (2.97) is equivalent to

753
$$Z^* = \frac{R_p}{1 + \omega^2 \tau_D^2} + \frac{iR_p \omega \tau_D}{1 + \omega^2 \tau_D^2}$$
 (2.100)

755 where

$$\tau_D = R_p C_p \tag{2.101}$$

is the Maxwell relaxation time (the reason for the subscript *D* is given below).

When normalized by the cell constant k (dimensions m⁻¹) the quantities A^* , Z^* and C^* and M^* become respectively the complex conductivity $\sigma^* = kA^*$, complex resistivity $\rho^* = Z^*/k$, complex relative permittivity $\varepsilon^* = kC^*/e_0 = C^*/C_0$ (where C_0 is the capacitance of the measuring cell in a vacuum, usually equated to that in air), and complex modulus M^* . Historically the same symbol has been used for the complex electric modulus defined in terms of measured circuit elements and as a material property, but this has not caused much (any?) confusion probably because the inverse capacitance V/q has never been considered as a physically useful quantity (in this respect it is not clear to this author why conductivity and resistivity should have separate physical uses either).

Series Resistance and Capacitance

For a resistance R_s in series with a capacitance C_s

773
$$Z*(i\omega) = R_s + \frac{1}{i\omega C_s} = R_s - \frac{i}{\omega C_s} = R_s \left(\frac{\omega \tau_E - i}{\omega \tau_E}\right),$$
 (2.102)

775
$$A*(i\omega) = \frac{R_s}{1+\omega^2 R_s^2 C_s^2} + \frac{i\omega R_s^2 C_s}{1+\omega^2 R_s^2 C_s^2} = \frac{R_s}{1+\omega^2 \tau_E^2} + \frac{i\omega R_s \tau_E}{1+\omega^2 \tau_E^2},$$
 (2.103)

777
$$C*(i\omega) = \frac{A*(i\omega)}{-i\omega} = C_s \left(\frac{1-i\omega R_s C_s}{1+\omega^2 R_s^2 C_s^2}\right) = C_s \left(\frac{1}{1+\omega^2 \tau_E^2} - \frac{i\omega \tau_E}{1+\omega^2 \tau_E^2}\right),$$
 (2.104)

779
$$M*(i\omega) = i\omega Z*(i\omega) = i\omega \left(R_s - \frac{i}{\omega C_s}\right) = i\omega R_s \left(\frac{\omega \tau_E - i}{\omega \tau_E}\right) = \frac{R_s}{\tau_E} \left(1 + i\omega \tau_E\right)$$
 (2.105)

where $\tau_E = R_s C_s$ that is generally not equal to $\tau_D = R_p C_p$.

The relations between the four response functions are conveniently summarized by [1,10]

2.2.8.3 Experimental Factors

Cable Effects

Cable impedances can be analyzed using transmission line methods that invoke an infinite number of $\{L,C\}$ components. One line of the cable is considered to be a series of inductances L and the other line as a zero impedance wire, with capacitances C connecting the two between every pair of inductances. In the limit of an infinite number of inductance and capacitance elements the cable impedance $Z_{cable} = \left(L/C\right)^{1/2}$ is real and constant. Coaxial cables are made so that C is 30 pF/ft and L is 0.075 μH /ft so that $Z_{cable} = \left(7.5 \times 10^{-8} \, H/3.0 \times 10^{-11}\right)^{1/2} = 50\Omega$. Thus a short cable with a 50 Ω resistor across it looks like an infinitely long cable and a 50 Ω load on the cable has an ideal impedance match for maximum power transfer. Such a cable will also behave as an inductor if short circuited so that for a high conductivity attached sample resonance effects may be significant.

Electrode Polarization

This occurs for two and three terminal measurements when charge transfer does not occur between an electrode and the sample material, i.e. when the applied voltage is less than the decomposition potential of the sample (four terminal measurements are immune to this but they do not produce reliable capacitance data and require separate sample preparation). In this case the electrode-sample contact can be approximated as a capacitance C_s in series with the sample [11-13] that is much larger than the sample capacitance C_p . If the amplitude of the applied potential is too large (above the decomposition potential of the electrolyte) a Faradaic impedance [14, 15] will also occur in parallel with this capacitance [16] that can sometimes be approximated as a Warburg impedance (see §2.4.3).

A series capacitance does not affect $M''(\omega)$ and simply adds $1/C_s$ to $M'(\omega)$: the total impedance $Z^*_{total}(i\omega)$ of the sample impedance $Z^*(i\omega)$ and C_s is $Z^*_{total}(i\omega) = Z^*(i\omega) + 1/i\omega C_s$ so that

813
$$M*(i\omega) = i\omega Z_{total}^* = i\omega Z*(i\omega) + 1/C_s.$$
 (2.107)

It is a considerable advantage of the electric modulus function that $M''(\omega)$ is unaffected by electrode polarization and other high capacitance phenomena. This is exploited in some of the methods of data analysis discussed below but it should be noted that some researchers have correctly noted that M^* also suppresses low frequency information (relative to ε^* for example), but it can equally be claimed that ε^* suppresses high frequency information. The low frequency

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high capacitance advantage of M^* is not shared by the imaginary component of the resistivity ρ "
because

823
$$\lim_{\omega \to 0} \rho''(\omega) \propto \lim_{\omega \to 0} \left(\frac{1}{k \omega C_s} \right) = \infty, \tag{2.108}$$

but the low frequency behavior of ρ' can be useful (see below).

Electrode polarization can however make the direct determination of the low frequency quantities ε_0 and σ_0 difficult and sometimes impossible because it increases ε' above ε_0 at low frequencies and, usually at lower frequencies, decreases σ' to below σ_0 . Overlap between bulk relaxations and these two electrode polarization effects prevents the observation of limiting low frequency plateaus in $\varepsilon'(\omega)$ and/or $\sigma'(\omega)$. Although relaxation of electrode polarization often occurs at much lower frequencies than the bulk relaxation,

$$\tau_{electrode} = \frac{\epsilon_0 C_s}{C_0 \sigma_0} >> \frac{\epsilon_0 C_p}{C_0 \sigma_0} = \tau_D, \tag{2.109}$$

the magnitude of the polarization dispersion can be very large [proportional to $(C_s - C_p) \approx C_s$] and its high frequency tail can extend well into the bulk relaxation region. This phenomenon is illustrated by the following representative average circuit quantities: a parallel capacitance $C_p = 10 \, \mathrm{pF}$ and parallel resistance $R_p = 10^7 \, \mathrm{ohm}$ in series with a polarization capacitance of $C_s = 10^4 \, \mathrm{pF}$. Because both R_p and C_p will have distributions in a typical electrolyte there will be dispersions in both ε' and σ' (see §2.4). The dispersion is centered around $\omega \approx 1/(R_p C_p) = 10^4 \, \mathrm{s^{-1}}$ and the low frequency plateau in ε' would normally then normally be seen at ca. $\omega \approx 10^2 \, \mathrm{s^{-1}}$, but this is dwarfed by the polarization capacitance at that frequency, $C_{pol}(\omega >> (R_p C_s)^{-1}) = C_s /(\omega^2 R_p^2 C_s^2) = 100 \, \mathrm{pF}$, an order of magnitude higher than C_p . On the other hand, the low frequency dispersion in conductivity due to polarization has barely begun at $\omega = 10^2$: $\sigma_{ele} / \sigma_0 = \omega^2 \tau_{ele}^2 / (1 + \omega^2 \tau_{ele}^2) = 0.99$ for $\omega \tau_{ele} = \omega R_p C_s = (10^2)(10^{-1}) = 10$, where the fact that the limiting high frequency conductivity for the Debye-like relaxation of electrode polarization is σ_0 :

849
$$\lim_{\omega \tau_{ele} \to \infty} \sigma_{ele}' = \frac{\left(\varepsilon_0 - \varepsilon_\infty\right)_{ele} e_0}{\tau_E} = \frac{\left(\varepsilon_0 - \varepsilon_\infty\right)_{ele} e_0 \varepsilon_\infty}{\tau_D \varepsilon_0} = \frac{\left(\varepsilon_0 - \varepsilon_\infty\right)_{ele} \sigma_0}{\varepsilon_0} \approx \sigma_0 \text{ for } \varepsilon_{0,ele}? \quad \varepsilon_{\infty,ele}$$
 (2.110)

Effects similar to electrode polarization can arise from other causes, such as poor electrode contact where a capacitance due to air gaps occurs in parallel with a resistance at the contact areas. Poor contacts have been shown to give spurious dielectric losses in undoped alkali halides

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[17], and is suspected to be responsible for the poor reproducibility of other dielectric data for alkali halides [18]. Space charge effects can also produce a series capacitance at the electrode [19,20].

2.3 Dielectric Relaxation

An excellent resource for dielectric relaxation is ref. [3], particularly Chapter One by N. E. Hill. An excellent review of dielectric relaxation phenomena in supercooled and glassy materials is given by Richert [21] that also includes references to modern measurement techniques.

2.3.1 Frequency Domain

2.3.1.1 Dipole Rotation

A freely rotating dipole in a sinusoidally varying electric field with an angular frequency ω low enough that the dipole can keep up with the field behaves as a pure capacitance C_{pure} . The current then lags the field by $\pi/2$ radians and the complex admittance is

869
$$A^* = i\omega C_{pure}$$
. (2.111)

If the dipole cannot keep up with the field because of friction with its environment it will lag by an additional angle δ and a component of the current appears in phase with the voltage and is measured as a resistance. Equation (2.94) is then replaced by

$$I_{C} = -V_{0}\omega C_{p} \cos(\omega t - \pi/2 - \delta)$$

$$= -V_{0}\omega C_{p} \Big[\cos(\omega t - \pi/2)\cos\delta + \sin(\omega t - \pi/2)\sin\delta\Big]$$

$$= -V_{0}\omega C_{p} \Big[\sin(\omega t)\cos\delta - \cos(\omega t)\sin\delta\Big],$$
(2.112)

- and the term $+V_0\omega C_p\cos(\omega t)\sin\delta$ in eq. (2.112) is seen to be in phase with the applied voltage
- $V = +V_0 \cos(\omega t)$. This in phase component is of course zero when $\delta = 0$. Comparing eq. (2.112)
- 879 with eqs. (2.95) and (2.96) reveals that

881
$$A^* = \omega C_{pure} \sin \delta + i\omega C_{pure} \cos \delta$$
 (2.113)

883 and

885
$$C^* = C' - iC'' = C_{pure} \cos \delta - iC_{pure} \sin \delta$$
 (2.114)

so that

889
$$G_p(\text{effective}) = \omega C_{pure} \sin \delta$$
 (2.115)

891 and

893
$$C_p(\text{effective}) = C_{pure} \cos \delta$$
. (2.116)

At low frequencies when the lag angle δ tends to zero the effective capacitance equals C_{pure} and $G_p = 0$, as must be. When normalized by the geometric capacitance associated with the cell constant k, $C_0 = e_0 / k$ where e_0 is the vacuum permittivity 8.854×10^{-12} F m⁻¹, the complex capacitance becomes the complex permittivity, $\varepsilon^* = C^*/C_0$ so that

$$\varepsilon^* = \varepsilon' - i\varepsilon'' \tag{2.117}$$

902 where

904
$$\varepsilon' = \frac{C_p}{C_0} \left(\varepsilon_0 - \varepsilon_\infty \right) \cos(\delta) + \varepsilon_\infty, \tag{2.118}$$

905
$$\varepsilon'' = \frac{G_p}{\omega \cdot C_0} = \frac{\sigma}{e_0 \cdot \omega} = \frac{C_p}{C_0} (\varepsilon_0 - \varepsilon_\infty) \sin(\delta), \qquad (2.119)$$

907 and

909
$$\tan \delta = \frac{\varepsilon''}{\varepsilon'} = \frac{G_p}{\omega C_p}$$
. (2.120)

Note that $\tan \delta$ is independent of the geometric capacitance C_0 and has the same frequency dependence as ε " but with a retardation time of $\left(\varepsilon_{\infty}^E/\varepsilon_0^E\right)^{1/2}\tau_E$ rather than τ_E . Equations (2.113) and (2.114) imply

915
$$A^* = i\omega C_0 \varepsilon^*$$
 (2.121)

917 so that

919
$$\sigma^* = kA^* = i\omega e_0 \varepsilon^*$$
 (2.122)

921 and

923
$$\rho^* = \frac{1}{\sigma^*} = \frac{1}{i\omega e_0 \varepsilon^*}$$
 (2.123)

The complex electric modulus M^* is defined as the reciprocal of ε^* :

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927
$$M^* = 1/\varepsilon^*$$
 (2.124)

928

929 so that

930

931
$$M^* = i\omega C_0 Z^* = i\omega e_0 \rho^*$$
. (2.125)

932

- The functions σ^* , ε^* , ρ^* and M^* are all analytical and their components all conform to the Cauchy-Riemann and Kronig-Kramers equations. The relationships between them are given in eq. (2.106).
- For a single relaxation time the (Debye) functions $\varepsilon^*(i\omega)$, $\varepsilon'(\omega)$ and $\varepsilon''(\omega)$ for dielectric relaxation are

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939
$$\varepsilon^*(i\omega) = \varepsilon_{\infty}^E + \frac{\left(\varepsilon_0^E - \varepsilon_{\infty}^E\right)}{1 + i\omega\tau_E},\tag{2.126}$$

940
$$\varepsilon'(\omega) = \varepsilon_{\infty}^{E} + \frac{\left(\varepsilon_{0}^{E} - \varepsilon_{\infty}^{E}\right)}{1 + \omega^{2} \tau_{E}^{2}},$$
 (2.127)

941

942 and

943

944
$$\varepsilon''(\omega) = \frac{\left(\varepsilon_0^E - \varepsilon_\infty^E\right)\omega\tau_E}{1 + \omega^2\tau_E^2},$$
 (2.128)

945

- where ε_0^E and ε_∞^E are defined in §2.1.1 as the limiting low and high frequency limits of $\varepsilon'(\omega)$ at constant electric field, respectively. Equations (2.127) and (2.128) yield a complex plane plot of ε'' vs ε' that is a semicircle centered on the real axis at $\varepsilon' = (\varepsilon_0^E + \varepsilon_\infty^E)/2$. This is found by eliminating $\omega \tau_E$ between equations (2.127) and (2.128) (see Appendix C in Chapter One for details).
- jou uctains).
- The corresponding Debye functions for $\sigma'(\omega)$ and $\sigma''(\omega)$ are

952
$$\sigma'(\omega) = e_0 \omega \varepsilon''(\omega) = \frac{e_0 \left(\varepsilon_0^E - \varepsilon_\infty^E\right) \omega^2 \tau_E}{1 + \omega^2 \tau_E^2}$$
 (2.129)

953

954 and

955

956
$$\sigma''(\omega) = e_0 \omega \varepsilon_{\infty}^E + \frac{e_0 \omega \left(\varepsilon_0^E - \varepsilon_{\infty}^E\right)}{1 + \omega^2 \tau_E^2}.$$
 (2.130)

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Thus the real part of the conductivity of a Debye dielectric increases from zero at low frequencies to a high frequency limit of

961
$$\sigma_{\infty} = \lim_{n \to \infty} \sigma'(\omega) = e_0 \left(\varepsilon_0^E - \varepsilon_{\infty}^E \right) / \tau_E,$$
 (2.131)

and the imaginary part diverges at high frequencies. Derivations of the Debye expressions for $M'(\omega)$ and $M''(\omega)$ are instructive and straightforward but tedious – they are given in Appendix

965 2.1. The results are

966
$$M'(\omega) = M_0^E + \frac{\left(M_\infty^E - M_0^E\right)\omega^2 \tau_E^2}{1 + \omega^2 \tau_E^2}$$
 (2.132)

968 and

970
$$M''(\omega) = \frac{\left(M_{\infty}^E - M_0^E\right)\omega\tau_E}{1 + \omega^2\tau_E^2},$$
 (2.133)

where
$$M_0^D = 1/\varepsilon_0^D$$
, $M_\infty^E = 1/\varepsilon_\infty^E$, and $(\varepsilon_\infty^E/\varepsilon_0^E)\tau_E = \tau_D$.

from the conductivity contribution

If a limiting low frequency conductivity σ_0 is present that is not physically related to the dielectric loss process (e.g. ionic conductivity in a dilute aqueous solution), it must be subtracted from the measured conductivity before the dielectric loss is calculated from eq. (2.128). Otherwise the limiting low frequency dielectric loss $\lim_{n\to 0} \varepsilon$ " $\to 0$ will be masked by the rapid rise

979
$$\lim_{\omega \to 0} \varepsilon'' = \lim_{\omega \to 0} \frac{\sigma_0}{e_0 \omega} \to \infty. \tag{2.134}$$

It has been argued that this subtraction is physically meaningful only if the conductivity is unrelated to the dielectric loss process (as in the aqueous solutions just mentioned). If the dielectric loss peak correlates with σ_0 as occurs in alkali silicate glasses [22-28] and other ionically conducting liquids and glasses then the subtraction of σ_0 can be regarded as artificial and other methods of data analysis are preferred (although this position is not universally held). This is the principle reason for not using the complex permittivity in analyzing highly conducting materials and is the subject of §2.4.

If the decay function is nonexponential then dielectric relaxation can be described in terms of a distribution of retardation times $g(\ln \tau_E)$ defined by the relations

$$\phi_E(t) = \int_{-\infty}^{+\infty} g(\ln \tau_E) \exp\left(-\frac{t}{\tau_E}\right) d\ln \tau_E$$
(2.135)

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992 993

and

994

995
$$\int_{-\infty}^{+\infty} g\left(\ln \tau_E\right) d\ln \tau_E = 1, \qquad (2.136)$$

997 so that eq. (2.126) generalizes to

998

996

999
$$\varepsilon^* - \varepsilon_{\infty}^E = \left(\varepsilon_0^E - \varepsilon_{\infty}^E\right) \int_{-\infty}^{+\infty} \frac{g\left(\ln \tau_E\right)}{1 + i\omega \tau_E} d\ln \tau_E.$$
 (2.137)

The generalization of eqs. (2.127) and (2.128) are

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1003
$$\varepsilon'(\omega) = \varepsilon_{\infty}^{E} + \left(\varepsilon_{0}^{E} - \varepsilon_{\infty}^{E}\right) \left[\int_{-\infty}^{-\infty} g\left(\ln \tau_{E}\right) \frac{1}{1 + \omega^{2} \tau_{E}^{2}}\right] d\ln \tau_{E} = \varepsilon_{\infty}^{E} + \left(\varepsilon_{0}^{E} - \varepsilon_{\infty}^{E}\right) \left\langle \frac{\omega \tau_{E}}{1 + \omega^{2} \tau_{E}^{2}}\right\rangle$$
(2.138)

1004 1005 and

1006

1007
$$\varepsilon''(\omega) = \left(\varepsilon_0^E - \varepsilon_\infty^E\right) \int_{-\infty}^{\infty} g\left(\ln \tau_E\right) \frac{\omega \tau_E}{1 + \omega^2 \tau_E^2} d\ln \tau_E = \left(\varepsilon_0^E - \varepsilon_\infty^E\right) \left\langle \frac{\omega \tau_E}{1 + \omega^2 \tau_E^2} \right\rangle. \tag{2.139}$$

1009 The n^{th} moments of a distribution function are

1010

1008

1011
$$\left\langle \tau_E^n \right\rangle = \int_{-\infty}^{+\infty} \tau_E^n g\left(\ln \tau_E\right) d\ln \tau_E$$
. (2.140)

1012

- If the integral $\int_{-\infty}^{+\infty} g(\ln \tau_E) d\ln \tau_E$ diverges, as it does for a constant phase angle impedance for
- 1014 example, $g(\ln \tau_E)$ is not renormalizable and a constant phase angle impedance can therefore be
- valid only over a limited range in relaxation times. In terms of $\phi(t)$ the moments are

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1017
$$\left\langle \tau_E^n \right\rangle = \frac{1}{\Gamma(\omega)} \int_0^{+\infty} t^{n-1} \phi(t) dt$$
 (2.141)

1018

1019 and

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$$1021 \qquad \left\langle \tau_E^{-n} \right\rangle = \left(-1\right)^n \left[\frac{d^n \left(\phi_E\right)}{dt^n} \right]_{t=0} \tag{2.142}$$

2.3.1.2 Ionic Hopping

Chapter One of [3] by N. E. Hill discusses the studies of Frohlich [6] and others on the dielectric relaxation consequences of two state models. We select here the Frohlich account of an entity that has only two possible equilibrium positions 1 and 2. The entity could be a molecular dipole or an ion for example. If the transition probabilities between the two positions are w_{12} and w_{21} when there is no applied field then a Debye relaxation with a single relaxation time is predicted that $\tau_E = 1/(w_{12} + w_{21})$ has Arrhenius dependence an temperature $\tau_E = A_E \exp(\Delta H / RT)$ where the pre-exponential factor A_E is a weak function of temperature and ΔH is the energy barrier that separates the two positions. As noted by Hill, however, a nonexponential decay function may result from local field effects.

2.3.2 Time Domain

Consider the case where an electric field E is "instantaneously" increased from zero to E_0 across a dielectric sample at time t=t' and kept constant thereafter, i.e. $E(t)=E_0h(t-t')$ where h(t) is the Heaviside function (eq. (1.327)). The initially randomized dipoles will partially orient themselves over time and the polarization and displacement will both increase (the final average orientation will not be complete because of thermal fluctuations):

$$D(t) = D(0) + \left[D(\infty) - D(0)\right] \left[1 - \phi_E(t)\right], \tag{2.143}$$

where D(0) and $D(\infty)$ are the limiting short time (high frequency) and long time (low frequency) values of D(t) and $\phi_E(t)$ is the decay function for polarization at constant E corresponding to D(t). The increase of D from zero to $D(\infty)$ is "instantaneous" compared with dielectric relaxation times (generally no shorter than about 10^{-11} s) and is due to polarization of molecular electron clouds that occurs roughly on optical time scales.

It is sometimes convenient to approximate the relation between time domain data and $\varepsilon''(\omega)$ by the *Hamon approximation*

1051
$$\varepsilon''(\omega) \approx \left(\varepsilon_0^E - \varepsilon_\infty^E\right) \left(\frac{-d\phi_E}{dt}\right) \left(\frac{5t}{\pi}\right),$$
 (2.144)

obtained from the simplification that the normalized displacement current is given by 1054

$$1055 \qquad \left(\frac{-d\phi_E}{dt}\right) \sim t^{-n} \,. \tag{2.145}$$

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No comparably simple relation exists between $\varepsilon'(\omega)$ and $\phi(t)$. Williams, Watt, Dev and North [29] have shown that for the Williams-Watt [30] decay function

1059

$$1060 \qquad \phi(t) = \exp\left[-\left(\frac{t}{\tau_0}\right)^{\beta}\right] \tag{2.146}$$

1061

the Hamon approximation is accurate within 1% for $\omega \tau_0 > 1$ but fails for $\omega \tau_0 \le 1$ and $\beta > 0.2$. Equation (2.144) therefore offers a high frequency approximation to the broadest frequency domain Williams-Watt functions that cannot be expressed in terms of named functions.

The complex relative permittivity $\varepsilon^*(\omega)$ is related to the derivative of $\varepsilon(t)$ by

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1067
$$\varepsilon^* (i\omega) - \varepsilon_{\infty}^E = \left(\varepsilon_0^E - \varepsilon_{\infty}^E\right) \int_0^{\infty} -\left(\frac{d\phi_E}{dt}\right) \exp(-i\omega t) dt$$
 (2.147)

1068

where $\varepsilon_0^E = D(\infty)/E_0$ and $\varepsilon_\infty^E = D(0)/E_0$. In the simplest case $\phi_E(t)$ is exponential,

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1071
$$\phi_E(t) = \exp\left[-\left(\frac{t}{\tau_E}\right)\right],$$
 (2.148)

1072

and insertion of eq. (2.148) into eq. (2.147) yields the Debye equations (2.127) and (2.128) [Chapter One of ref. 3].

1075

1076 2.3.3 Temperature Domain

relation

1077 1078 In many situations ω and τ_E are approximately interchangeable variables. Since τ_E often varies strongly with temperature a narrow temperature range can be used as a surrogate for a wide frequency range. The temperature dependence of τ_E is often approximated by the Arrhenius

1079 1080 1081

$$1082 \tau = \tau_0 \exp\left(\frac{E_a}{RT}\right), (2.149)$$

1083

where τ_0 is independent of temperature, R is the ideal gas constant, and E_a is the activation energy. A better approximation is the Fulcher equation

$$\tau_E = A_F \exp\left(\frac{B_F}{T - T_0}\right) \tag{2.150}$$

where A_F , B_F and T_0 are positive constants. Thus the variables $\ln(\omega\tau)$ at constant ω , and E_a/RT or $B_F/(T-T_0)$, are equivalent for a single relaxation time dielectric. In this case eqs. (2.149) and (2.150) indicate that over the convenient temperature range from liquid nitrogen (77 K) to room temperature (300K) the retardation time can vary over a very large range. For example τ changes by a factor of 10^{25} for an average activation energy of 50 kJ/mol. The temperature variable is therefore extremely useful for scans of the total relaxation spectrum and is frequently used for polymers whose relaxation behavior is typically characterized by widely separated and broad relaxation processes. Activation energies E_a are obtained from plots of log frequency $\ln f$ against the inverse temperature $1/T_{\rm max}$ at which ε " or $\tan \delta$ passes through its maximum:

1099
$$\left\langle \frac{E_a}{R} \right\rangle = -\left[\frac{d \ln f}{d \left(1/T \right)} \right].$$
 (2.151)

It has been reported [32] that the activation energy obtained in this way is ambiguous because it depends on whether the derivative is determined in the isothermal frequency domain or in the temperature domain at constant frequency: the frequency domain plot of $\ln f_{\rm max}$ vs. 1/T was found to be strongly curved whereas the plot of $\ln f$ vs. $1/T_{\rm max}$ was found to be linear.

Although temperature is useful because of its experimental convenience it is not quantitative because "everything changes with temperature". For example the dispersion $\left(\mathcal{E}_0^E - \mathcal{E}_\infty^E\right)$ can only be estimated because \mathcal{E}_0^E and to a less extent \mathcal{E}_∞^E are temperature dependent, although it can be estimated from the relation [33]

1110
$$\left(\varepsilon_0^E - \varepsilon_\infty^E\right) \approx \left(\frac{2}{\pi R}\right) \left\langle \frac{1}{E_A} \right\rangle^{-1} \int_0^\infty \varepsilon''(T) d(1/T).$$
 (2.152)

- However eq. (2.152) is approximate because of two assumptions in its derivation that must be made for mathematical tractability: (i) $\left(\varepsilon_0^E \varepsilon_\infty^E\right)$ is independent of temperature [32] and (ii)
- $\langle E_a \rangle = \langle 1/E_a \rangle^{-1}$ that is not generally true because of the Schmidt inequality (Chapter One)

$$1116 \qquad \langle E_A \rangle \langle 1/E_A \rangle^{-1} \ge 1. \tag{2.153}$$

The approximation is clearly better for smaller temperature ranges. There are two situations where $\ln \omega$ and E_{α}/RT are not even approximately equivalent however: (i) functions for which ω and τ_E are not invariably multiplied together (for example the conductivity of a Debye dielectric, eq. (2.128)); (ii) distributions of retardation times that change with temperature.

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1123 2.3.4 Equivalent Circuits

The electrical response for an exponential dielectric decay function, the Debye relations eqs. (2.127) and (2.128) plus any separate conductivity contribution σ_0 , is simulated by an equivalent circuit comprising three parallel arms: a capacitance C_p , a series combination of R_s and C_s , and a resistance R_p . The relaxation part of the circuit is the series component $R_s + C_s$, the parallel resistance R_p corresponds to the separate conductivity, and the parallel capacitance C_p simulates the limiting high frequency permittivity. If for a particular range of frequencies the equivalent circuit of an experimental sample resembles $R_s + C_s$ and the frequency range encompasses $\omega = 1/(R_s C_s)$ then a dielectric loss peak will be observed in that frequency range. An example is electrode polarization in a conducting medium that at low frequencies is approximated by an electrode capacitance in series with the low frequency resistance of the sample. In this case a dielectric loss is observed with a retardation time given by the product of the polarization capacitance and sample resistance. Electrode polarization effects in solid electrolytes can often be a serious problem; they were briefly discussed in §2.2.8.3 and are discussed in detail in §2.3.6.1 and §2.3.6.4 below.

In terms of the equivalent circuit the components of the complex permittivity are (see Appendix 2.3)

1141
$$\varepsilon'(\omega) = \frac{\sigma''}{e_o \omega} = \left(\frac{1}{C_o}\right) \left(C_p + \frac{C_s}{1 + \omega^2 \tau_p^2}\right)$$
 (2.154)

1143 and

1145
$$\varepsilon''(\omega) = \frac{\sigma'}{e_0 \omega} = \left(\frac{C_s}{C_0}\right) \left(\frac{\omega \tau_E}{1 + \omega^2 \tau_E^2}\right) + \frac{\sigma_0}{e_0 \omega}, \qquad (2.155)$$

that reproduce the Debye relations eqs. (2.127) and (2.128). The low and high frequency limits of ε ' are

1150
$$\lim_{\omega \to 0} \varepsilon'(\omega) = \varepsilon_0 = \left(\frac{C_p + C_s}{C_0}\right)$$
 (2.156)

1152 and

1154
$$\lim_{\omega \to \infty} \varepsilon'(\omega) = \varepsilon_{\infty} = \left(\frac{C_p}{C_0}\right). \tag{2.157}$$

1156 Matlab®/GNUOctave codes for computing $M^*(i\omega)$ and $\rho^*(i\omega)$ with the added R_p are given in

Appendix 2.2. A notable result is that $M^*(i\omega)$ exhibits two relaxations corresponding to the Debye relaxation and an additional relaxation due to σ_0 . The Debye relaxation for $M^*(i\omega)$ is unaffected by R_p but the conductivity relaxation due to σ_0 is.

As noted in §2.1 the occurrence of a dielectric and conductivity relaxation together raises an important nomenclature issue that has produced much confusion: the subscripts for denoting limiting low and high frequency limits can be ambiguous because these limits can refer to either the average dielectric relaxation frequency or to the average conductivity relaxation frequency. In particular, the quantity ε_{∞} that enters into the expression for the conductivity relaxation time, $\left\langle \tau_{D} \right\rangle = e_{0}\varepsilon_{\infty} / \sigma_{0}$, is the *high* frequency limit for the *conductivity* relaxation, that may correspond to the *low* frequency limit for a separate dielectric relaxation. A proposed nomenclature to resolve this ambiguity was given above in §2.1 and has already been used in this section.

2.3.5 Interfacial Polarization

In a homogeneous material $\nabla g \mathbf{D} = e_0 \varepsilon \nabla g \mathbf{E} = 0$ implies $\nabla g \mathbf{E} = 0$. At the interface between two dielectric materials of different permittivity, however, there is a discontinuity in ε and $\nabla g \mathbf{D} = 0$ no longer implies $\nabla g \mathbf{E} = 0$. The solution to this problem is obtained by applying Gauss's and Stokes' theorems to the interface with the result that the component of \mathbf{E} tangential to the interface is continuous across the interface and the normal component of \mathbf{D} is either continuous (no interfacial charge) or discontinuous if there is a free charge that is not the result of polarization of the materials on each side of the interface. These boundary conditions make macroscopic interfacial effects dependent on the geometry of the interface.

Relaxation of interfacial polarization between alternating slabs of insulating dielectric and conducting layers, generically referred to as a *Maxwell Layered Dielectric*, is characterized by a single relaxation time τ_i given by

1182
$$\tau_i = R_s C_s = \left(\frac{1_R}{1_C}\right) e_0 \rho \varepsilon = \left(\frac{1_R}{1_C}\right) \left(\frac{e_0 \varepsilon}{\sigma}\right)$$
 (2.158)

where 1_R is the thickness of the resistive layer with material resistivity ρ and 1_C is the thickness of the capacitive layer with material permittivity ε .

2.3.6 Maxwell-Wagner Polarization

Relaxation of interfacial polarization between a conducting sphere embedded in a dielectric continuum is known as *Maxwell-Wagner* (MW) *polarization*. Wagner [34] computed the loss tangent $(\tan \delta)$ for a volume fraction ϕ of spheres of material conductivity σ_1 and relative permittivity ε_1 suspended in a dielectric medium of relative permittivity ε_2 , that was then generalized by Sillars [35] to suspensions of nonspherical particles. An excellent discussion of the phenomenon is given in ref [3] from which much of the following is distilled. We also draw from the paper by van Beek [36] who gave the Sillars formula and then considered the special case of suspended spheres, and noted that the often cited Wagner formula is only correct when the

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1196 permittivities of the suspended material and the dielectric medium are equal and that the Sillars 1197 expression does not have this flaw.

The Sillars expression for aspherical particles with aspect ratio a/b and a parallel to the field direction is

1199 1200

1198

1201
$$\tan \delta = \frac{\varepsilon_2 K}{\left[\mathbf{e}_{\infty} \left(\varepsilon_2 K + \mathbf{e}_{\infty}\right)\right]^{1/2}} \left(\frac{\omega \tau_0}{1 + \omega^2 \tau_0^2}\right),$$
 (2.159)

1202

1203 with

1204

$$K = \frac{n^2 \phi \varepsilon_2}{\left[\left(n - 1 \right) \varepsilon_2 + \varepsilon_1 \right]} \tag{a},$$

 $\mathbf{e}_{\infty} = \varepsilon_2 \left[1 + \frac{n\phi(\varepsilon_2 - \varepsilon_1)}{(n-1)\varepsilon_2 + \varepsilon_1} \right]$ 1205

 $T = \frac{\mathbf{e}_0 \left[\left(n - 1 \right) \varepsilon_2 + \varepsilon_1 \right]}{\sigma_1}$

$$\tau_0 = \frac{T}{\left\{ \left(\varepsilon_1 K + \mathbf{e}_{\infty} \right) / \mathbf{e}_{\infty} \right\}^{1/2}} \qquad (d),$$

1206

1207 where n is a function of the aspect ratio a/b. The limiting values for n are

1208

$$n:1$$
 $(a < b)$ (a)

1209

$$(a=b) (b)$$

(2.160)

$$n: 1 \qquad (a < b) \qquad (a)$$

$$n = 3 \qquad (a = b) \qquad (b)$$

$$n \approx \left\{ \frac{a^2}{b^2 \left[\ln(2a/b) - 1 \right]} \right\} \qquad (a > b) \qquad (c),$$

1210

- Equation (2.161)(c) indicates that for needle-like particles oriented in the direction of the field the 1211 value of n can be large – for example $n \sim 50$ for a = 10b. Because $\tan \delta$ is roughly proportional to 1212
- n^2 [eqs. (2.159) and (2.160)a] the Maxwell-Wagner-Sillars effect can produce very large 1213
- dielectric losses. For spherical particles 1214

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$$K = \frac{9\phi\varepsilon_2}{\left[2\varepsilon_2 + \varepsilon_1\right]}$$
(a),
$$1216 \qquad \mathbf{e}_{\infty} = \varepsilon_2 \left[1 + \frac{3\phi\left(\varepsilon_2 - \varepsilon_1\right)}{2\varepsilon_2 + \varepsilon_1}\right]$$
(b),
$$T = \frac{\mathbf{e}_0\left[2\varepsilon_2 + \varepsilon_1\right]}{\sigma_1}$$
(c),

and τ_0 is again given by eq. (2.160)d. The maximum value of $\tan \delta$ computed from eq. (2.159)d

is therefore

1221
$$\tan \delta_{\text{max}} = \frac{\varepsilon_2 K}{2\left[e_{\infty}\left(\varepsilon_2 K + e_{\infty}\right)\right]^{1/2}}$$
 (2.163)

1223 This expression is inconveniently complicated but simplifies when $\phi \rightarrow 0$:

1225
$$\lim_{\phi \to 0} \left(\tan \delta_{\max} \right) = \frac{9\phi \varepsilon_2}{2(2\varepsilon_2 + \varepsilon_1)}. \tag{2.164}$$

The components of the complex relative permittivity for the Maxwell-Wagner phenomenon for this limiting case are conveniently expressed using three ancillary functions [36]:

1230
$$\varepsilon_{\phi} = \varepsilon_{2} \left\{ 1 + \frac{3\phi(\varepsilon_{1} - \varepsilon_{2})}{2\varepsilon_{2} + \varepsilon_{1}} \right\}, \tag{2.165}$$

1232
$$S = \frac{9\phi\varepsilon_2}{2\varepsilon_2 + \varepsilon_1},$$
 (2.166)

$$1234 T = \frac{\sigma_1}{e_0 \left(2\varepsilon_2 + \varepsilon_1\right)}. (2.167)$$

1236 Then

1238
$$\varepsilon'' = \frac{\left(\varepsilon_{\phi} S \omega T\right)}{1 + \omega^2 T^2} \tag{2.168}$$

1240 and

1242
$$\varepsilon' = \varepsilon_{\phi} \left\{ 1 + \frac{S}{1 + \omega^2 T^2} \right\}. \tag{2.169}$$

1243

1244 The maximum in the observed dielectric loss ε_{MW} is therefore

1245

1246
$$\varepsilon_{\text{max}} = \frac{9\phi\varepsilon_2^2}{2(2\varepsilon_2 + \varepsilon_1)} \left[1 + \frac{3\phi(\varepsilon_2 - \varepsilon_1)}{2\varepsilon_{12} + \varepsilon_1} \right] \rightarrow \frac{9\phi\varepsilon_2^2}{2(2\varepsilon_2 + \varepsilon_1)}, \tag{2.170}$$

1247

1248 that occurs at an angular frequency ω_{max} given by

1249

1250
$$\omega_{\text{max}} = 1/\tau_{MW} = \frac{\sigma_1}{e_0 \left(2\varepsilon_1 + \varepsilon_2\right)}. \tag{2.171}$$

1251

- 1252 At ω_{max} the value of ε' from eq. (2.169) is $\lim_{\phi \to 0} \varepsilon' = \varepsilon_2$ that when combined with eq. (2.170)
- 1253 produces eq. (2.164).

1254

1255 2.3.7 Examples

Attention is restricted to the dielectric relaxation of water molecules in different environments.

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2.3.7.1 Liquid Water

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Water is one of the few liquids that relaxes with a single retardation time (or very close to it) and therefore has a Debye complex permittivity. Its dielectric relaxation frequency depends on temperature but always lies within the microwave region of the em spectrum. This has important implications for both navigational and meteorological radar and is of course the basis for microwave cooking. The temperature dependence of the retardation time is not Arrhenius but rather adheres to the empirical Fulcher equation (1.543) and (2.150), repeated here for convenience:

1266 1267

1268
$$\tau = A_F \exp\left(\frac{B_F}{T - T_0}\right),\tag{2.172}$$

- with parameters $A_F = 1.25 \times 10^{-13}$ s, $B_F = 669$ K, $T_0 = 138$ K that give a good description of $\tau(T)$
- down to the limit of supercooling of bulk water, ca. -35° C. The relaxation frequency $(1/2\pi\tau)$
- therefore varies between 62 GHz at 0° C and 74 GHz at 100 °C and the energy absorption at 100
- 1273 °C is about 75% that at 0 °C. Microwave ovens generally operate at a frequency 2.45 GHz that
- lies on the low frequency side of the Debye dielectric loss peak the dielectric losses at this
- frequency are about 4.0% and 3.3% of the maximum loss. The fact that the frequency of a

microwave oven is on the lower side of the dielectric loss peak of water means that energy absorption decreases with increasing temperature as the loss peak moves to higher frequencies, thus preventing runaway heating.

2.3.7.2 Supercooled Water

Maxwell-Wagner polarization has been used to obtain the relative permittivity of supercooled water down to about -35 0 C [37, 38]. The Maxwell-Wagner losses occur in the frequency range 10^{5} – 10^{6} Hz that is far below the frequency range for the dielectric relaxation of water (around 10^{11} Hz) so that the measured values for the relative permittivity correspond to the limiting low frequency value $\varepsilon_0 >: 80$. This range is also far above the relaxation frequency for ice that is about $10^{3.5}$ Hz at 0° C and decreases with decreasing temperature, so that if crystallization occurred the relevant relative permittivity of ice is the limiting high frequency value ε_{∞} : 5, far smaller than the limiting low frequency value ε_{0} >: 80 It is fortunate that the Maxwell-Wagner losses occur at frequencies between the relaxation frequency ranges of water and ice and do not overlap with either.

Emulsions of water in heptane stabilized by the surfactant sorbitol tristearate [37] and droplets suspended in beeswax [38] both exhibit Maxwell-Wagner polarization. In the first and rigorous beeswax study by Hasted and Shahidi [38] volume fractions of 0.5% and 1.0% were used. Hodge and Angell [37] later used a much larger volume fraction of water (30%) that was necessitated by their much lower instrumental sensitivity. Their data were stated to be inconsistent with the Maxwell-Wagner formulae because the observed values of ε''_{max} were claimed to be about four times larger than predicted and their sign of $(d\varepsilon''_{max}/dT) \propto (d\varepsilon_1/dT)$ was positive rather than negative as predicted by their eq. (3). However their eq. (3) is incorrect – the numerator term ε_2^2 of eq. (2.170) was given as ε_1^2 so that the analyses of ε_{MW}^* given in [1] and [37] are both incorrect. Equation (2.170) predicts that ε''_{max} is indeed inversely proportional to ε_1 if ε_1 ? ε_2 (a good approximation for water droplets in hexane). The analyses in terms of the electric modulus [1,37] are unaffected by this mistake and remain valid although the stated requirement that a series capacitance that simulates the surfactant layer around the droplet needs to be large for the modulus analysis to be useful [1] is not correct (see eq. (2.107) above).

The observed maxima in ε " decreased with decreasing temperature that is consistent with eq. (2.170), but for $\varepsilon_1 \approx 100$? $\varepsilon_2 \approx 2$ and $\phi = 0.3$ the predicted value is about $\varepsilon_{\text{max}} \approx \left\{ (9)(0.3)(4)/[2(106)] \right\} \approx 0.005$, compared with the experimental values that range between about 0.4-0.8. The observed value is therefore too large by a factor of about 100. Also, the measured ratio of ε_{max} at the temperature extremes of 0°C and -35°C is about 1.8 compared with the correct value of about 1.2. The observed values of ω_{max} for ε " were centered around $2\pi \left(5.5 \times 10^6 \, Hz\right) \approx 3.5 \times 10^7 \, \text{rad/s}$ from which eq. (2.171) predicts a conductivity of about

1312
$$\sigma_1 \approx e_0 \left[\left(2\varepsilon_1 + \varepsilon_2 \right) + \phi \left(\varepsilon_1 - \varepsilon_2 \right) \right] \omega_{\text{max}} / \left(1 - \phi \right) \approx \left(9 \times 10^{-12} \text{ F/m} \right) \left(230 \right) \left(3.5 \times 10^7 \right) / 0.7$$

 $\approx (9 \times 10^{-12} \text{ F/m})(230)(3.5 \times 10^7) / 0.7 \approx 0.1 \text{ S/m}$, that is impossibly high.

The measured modulus peak heights also decreased with decreasing temperature and since

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1315 M''_{max} is assumed to be inversely proportional to the permittivity this trend is also in the correct direction. Values of ε_1 for water were then derived by assuming that $M''_{\text{max}} \propto 1/\varepsilon_1$, fixing the 1316 proportionality constant from literature data for $arepsilon_1$ at 0 $^0\mathrm{C}$ and then least squares fitting a 1317 quadratic in temperature to eight data points between 0°C and -35 °C. Agreement with the earlier 1318 results, of which the authors were unaware at the time of paper submission (see Note added in 1319 1320 *Proof* in [37]), was within the $\pm 2\%$ uncertainties claimed for each method but the agreement is better than this because most of the discrepancies are systematic due to the different values of ε_1 1321 at 0°C for the two methods (measured in [38] but chosen from the literature as a proportionality 1322 1323 constant in [37]). When this is corrected for by equating the average of the modulus derived 1324 permittivities to the average from reference [38] the differences are reduced to 0.5% or less. This 1325 is a remarkable result given the simplifications used in the modulus analysis.

These Maxwell-Wagner results can be rationalized in terms of a simplified equivalent circuit for the emulsified water droplets: a parallel (R_1C_1) element (corresponding to the water droplet with relative permittivity ε_1 and conductivity σ_1) is in series with a capacitance C_s that simulates the suspected thin layer of emulsifier, and a capacitance C_2 in parallel with the series combination to simulate the surrounding heptane. Intuitively C_2 is much smaller than C_1 from both geometrical and physical considerations ($\varepsilon_2 = \varepsilon_1$). The circuit analysis is:

1332 (i) Admittance A_1 of parallel (R_1C_1) element:

1333
$$A_1 = 1/R_1 + i\omega C_1 = (1 + i\omega R_1 C_1)/R_1 = (1 + i\omega \tau_1)/R_1$$
 so that

1335
$$Z_1 = R_1 / (1 + i \omega \tau_1).$$
 (2.173)

1337 (ii) Impedance of $\{(R_1C_1)+C_s\}$ arm = $Z_{1s} = \frac{R_1}{1+i\omega\tau_1} + \frac{1}{i\omega C_s} = \frac{i\omega R_1C_s + 1 + i\omega\tau_1}{i\omega C_s(1+i\omega\tau_1)} \Rightarrow$

1339 $A_{1s} = \frac{i \omega C_s (1 + i \omega \tau_1)}{1 + i \omega (\tau_1 + R_1 C_s)}.$ (2.174)

1341 (iii) Admittance A_{1s2} of complete circuit:

1342
$$A_{1s2} = A_{1s} + i\omega C_2 = \frac{i\omega C_s - \omega^2 C_s \tau_1 + i\omega C_2 \left[1 + i\omega \left(\tau_1 + R_1 C_s\right)\right]}{1 + i\omega \left(\tau_1 + R_1 C_s\right)} =$$

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$$\frac{i\omega(C_s + C_2) - \omega^2(C_s\tau_1 + C_2\tau_1 - R_1C_sC_2)}{1 + i\omega(\tau_1 + R_1C_s)}.$$
 (2.175)

1345

1346 (iv) For $C_2 = C_1$ appropriate for water droplets in heptane the total admittance simplifies to

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1348
$$A_{1s2} = \frac{i \omega C_s - \omega^2 R_1 C_1 C_s}{1 + i \omega R_1 (C_1 + C_s)}.$$
 (2.176)

1350 Thus

$$C_{1s2}^{*} = \frac{A_{1s2}}{i\omega} = \frac{C_{s} (1 + i\omega R_{1}C_{1})}{1 + i\omega R_{1}C_{s}} = \frac{C_{s} (1 + i\omega R_{1}C_{1})(1 + i\omega R_{1}C_{s})}{1 + \omega^{2}R_{1}^{2}C_{s}^{2}}$$

$$= \frac{C_{s} - \omega^{2}R_{1}^{2}C_{1}C_{s}}{1 + \omega^{2}R_{1}^{2}C_{s}^{2}} + \frac{i\omega C_{s}R_{1}(C_{1} + C_{s})}{1 + \omega^{2}R_{1}^{2}C_{s}^{2}}$$

$$(2.177)$$

1354 so that

1356
$$C'' = \frac{\omega C_s R_1 \left(C_1 + C_s \right)}{1 + \omega^2 R_1^2 C_s^2}.$$
 (2.178)

 The maximum value $(C_1 + C_s)/2$ for C'' is therefore determined in part by the surfactant layer and is greater than the value $C_1/2$ for no series capacitance. This is consistent with the observed maxima in ε'' [37] being about 100 times greater than that calculated from the Maxwell-Wagner expression. The maximum in C'' also occurs at $\omega_{\max} = 1/(R_1 C_s)$ that is also determined in part by the surfactant layer and therefore would give an incorrect value for the conductivity of water. This dependency of the relaxation time on C_s can also account for the (unreported) fact that changing the suspending medium changed ω_{\max} [37] since the suspending medium would be expected to affect the surfactant layer and C_s .

The imaginary component of the electric modulus for the same circuit when $C_2 = C_1$ is

1368
$$M'' = \frac{i \omega R_1}{\left(1 + i\omega^2 R_1^2 C_1^2\right)} = \left(\frac{1}{C_1}\right) \frac{i \omega R_1 C_1}{\left(1 + i\omega^2 R_1^2 C_1^2\right)},$$
 (2.179)

the maximum value of which is $1/(2C_1)$ and therefore contains the desired information about C_1 that is independent of C_s . The frequency of maximum M'' is $\omega_{\text{max}} = 1/(R_1C_1)$ and is also independent of C_s .

Matlab® and GNUOctave calculations of the relaxation functions for the circuit enable values of the circuit elements to be quickly estimated that produce trends that are generally consistent with the experimental data, with the notable exception of the maximum values of ε " (discussed briefly below). For example good agreement with the experimental trends is attained with $R_1 = 10^3 \,\Omega$; $C_1 = 10^{-3} \,\mathrm{F}$; $C_2 = 10^{-5} \,\mathrm{F}$; $C_s = 5 \times 10^{-4} \,\mathrm{F}$. The value of 100 for the ratio C_1/C_2 was chosen to approximate the ratio of permittivities of water and hexane and to accommodate an unknown geometric factor for the suspending medium relative to the droplet, and the value of C_s

was found from the experimental ratio of 0.5 for the frequencies of maximum ε " and M" (the latter being higher). The geometric factor is probably the largest source of uncertainty in estimating the values of the circuit parameters.

The Maxwell-Wagner equivalent circuit discussed here is obviously crude but serves to rationalize the remarkable success of the electric modulus in analyzing the Maxwell-Wagner effect for water droplets in a dielectric medium of low permittivity.

2.3.7.3 Hydration Water

Water of ionic hydration is readily probed by dielectric relaxation if the ionic conductivity contribution to ε " and $\tan \delta$ is sufficiently small, such as often occurs in hydrate glasses. Data for $\text{Ca}(\text{NO}_3)_2$ hydrate glasses [39] provide a convenient illustration of how water in different molecular environments can be distinguished dielectrically. Spectra of dielectric $\tan \delta$ vs. 1/T at 1 Hz were shown for eight glasses of composition $\text{Ca}(\text{NO}_3)_2$. $R\text{H}_2\text{O}$ (R = 3, 4, 5, 6, 8, 10, 12, 14). Glasses with lower R values required the addition of KNO_3 to ensure glass formation but this was expected to have only a minor effect on water dynamics because water was expected to be much more strongly bound to Ca^{2+} because of its larger ionic charge/radius compared with K^+ . Four relaxations were observed labeled as α , β , γ , δ :

- (α) A conductivity relaxation at low 1/T corresponding to the onset of conductivity at glass transition was manifested as a steep increase in $\tan \delta$. The relaxation temperature corresponds to $\tan \delta = 1$ and will be referred to here as the "conductivity wing". It is essential that this relaxation occur at sufficiently high T in order that the other relaxations occur in the poorly conducting glassy state and not be hidden beneath the conductivity contribution to $\tan \delta$.
- 1402 (β) A dielectric relaxation lying close to the conductivity wing whose shift in position with R paralleled that of the conductivity relaxation. It was observable only as a shoulder for R = 1-6 and (probably) R = 10 but is seen as a distinct peak for $R \approx$ trace.
- (γ) A weak low temperature dielectric relaxation $(\tan \delta_{\text{max}} \approx 10^{-3} 10^{-2})$ was observed as a 1406 broad maximum for R = 4, 5, 6 and as a shoulder for $R \ge 8$.
- 1407 (δ) A dielectric relaxation whose intensity increased rapidly with R. It was probably a part of the broad maximum near $10^3 / T \approx 7.5$ for R = 8 but appeared as a clear maximum for $R \ge 10$.

The β relaxation was assigned to cation bound water that for the reason given above probably coordinates Ca⁺ rather than K⁺. The rapid shift in relaxation temperature with R > 1 was interpreted as a change in water dynamics as H₂O replaces NO₃⁻ in the first coordination shell of Ca⁺. The R - invariance for R = trace and R = 1 was attributed to a single water molecule lying in the first coordination shell. This assignment of the β relaxation to Ca²⁺ bound water implied a dielectric activity that merits discussion. The most plausible geometry for H₂O coordinated to Ca⁺ is when the H₂O dipole points away from the Ca+ ion. However if this held in the complex ionic environment of the glass there would be no dielectric activity because the rotational axis would bisect the H-O-H angle and coincide with the dipole vector. Two alternatives suggest themselves:

(1) Exchange of water and nitrate in the coordination shell. This implies an associated volume fluctuation and ultrasonic activity. Such activity has been observed [40,41] in $Ca(NO_3)_2 \cdot RH_2O$

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solutions at about 20 MHz at room temperature. This relaxation moved to higher frequencies with increasing R and the edge of a second relaxation at higher frequencies was noted, both being consistent with the glassy state dielectric behavior. Such an exchange would also be expected to contribute to the translational ionic migration that produces conductivity, consistent with the essentially R – invariant difference between the α and β relaxation temperatures. The possibility that this relaxation is part of a conductivity relaxation with a distribution of relaxation times is discussed in §2.5.

A different Ca+-OH, geometry in which the dipole vector and rotation axis do not (2) coincide. Neutron diffraction data indicate this occurs in CaCl₂ and NiCl₂ solutions [42], in which an angle of ca. 40° was observed between the dipole and coordination axes at R=12.6(NiCl₂) and 12.3 (CaCl₂), and about 0° in dilute solutions ($R \approx 450$). It was not possible to find the dielectric activity per water molecule of the β relaxation in the Ca(NO₃)₂·RH₂O glasses because of overlap with the conductivity wing and the γ relaxation, but for the mixed nitrate glasses the well defined conductivity wing for the anhydrous mixture could be shifted and subtracted to yield plausibly shaped peaks of $\tan \delta$ vs. 1/T. The peak heights and widths in the R = 1 and R = 3 glasses were about the same so that barring an unlikely ratio of activation energies in excess of 3 it appears that the dielectric activity per water molecule does indeed decrease with increasing R. A crude calculation yielded sensible values of $\Delta\theta$ from the observed values of $\tan \delta_{\max}$: the dipole being relaxed was assumed to be the component of the water dipole $(\mu_{\scriptscriptstyle W})$ orthogonal to the rotation axis, magnitude $\mu_{W} \sin(\Delta \theta)$, and $\tan \delta_{max}$ was assumed to be proportional to $(\varepsilon_0 - \varepsilon_\infty)$ that is in turn proportional to $R \left[\mu_W \sin(\Delta \theta) \right]^2$. Equating $\tan \delta_{\max}$ for the 1R and 3R glasses then yielded

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$$\frac{3}{T_{3R}}\sin^2(\Delta\theta_{3R}) = \frac{1}{T_{1R}}\sin^2(\Delta\theta_{1R}),$$
 (2.180)

1445 so that

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1444

1447
$$\sin^2(\Delta\theta_{3R}) \approx 0.286 \sin^2(\Delta\theta_{1R})$$
. (2.181)

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Examples of $\{\Delta\theta_{1R}, \Delta\theta_{3R}\}$ pairs were $\{60^{\circ}, 28^{\circ}\}$ and $\{30^{\circ}, 15^{\circ}\}$, both sensible values and roughly comparable with the neutron diffraction values.

For large values of R the δ relaxation was expected to resemble that of pure water so that an extrapolation to infinite dilution could yield the temperature at which the relaxation frequency of water is 1 Hz. The retardation temperatures at 1 Hz for the δ relaxation in four glasses (Ca(NO₃)₂, CaZnCl₄, Li₂ZnCl₄ and ZnCl₂ hydrates) all extrapolated to 162 ± 5 K at infinite dilution, suggesting that the relaxation temperature for pure water would be 162 ± 5 K at 1Hz. The temperature dependence of the relaxation time for water between -20°C to +30°C [43] was found to follow the Fulcher equation

1459
$$\tau(T) = A_F \exp\left(\frac{B_F}{T - T_0}\right) \tag{2.182}$$

with $A_F = 1.25 \times 10^{-13}$ s, $B_F = 669$ K, $T_0 = 138$ K. The extrapolated {1 Hz, 162 ± 5 K} datum agreed with the predicted Fulcher value {1 Hz, 162 K}. Given the large extrapolation over about 11 orders of magnitude (!) this agreement constitutes good evidence that dielectric relaxation of water outside the first coordination shell of the Ca^{2+} and Li^+ cations is the same as pure water. This was supported by a similar extrapolation of LiCl in glycerol data that yielded a relaxation temperature equal to the directly observable value for pure glycerol at 1 Hz.

- 2.4 Conductivity Relaxation
- 2.4.1 General Aspects

As noted earlier relaxation of polarization can occur either by translation of electric charge (electric current), or by dipole rotation/localized ion hopping (displacement current). Thus polarization induced by an electric field can occur by *conductivity relaxation* [44] arising from long range translational migration of point charges as well as by the dielectric relaxation considered so far. The time scale associated with a frequency invariant conductivity σ_0 is defined by (eq. 1.42)

1477
$$\langle \tau_D \rangle = \sigma_0 / e_0 \varepsilon_\infty$$
, (2.183)

but this is not evident in σ' vs $\ln \omega$ plots nor is it for the function $\varepsilon^* = \varepsilon' - i\sigma_0 / e_0 \omega$. However ρ'' and M'' clearly indicate the time scale because they exhibit maxima in the frequency domain at $\omega \approx 1/\langle \tau_D \rangle$. The time constant τ_D in eq. (2.183) differs from the characteristic time τ_e in the Fermi gas expression for electronic conductivity in metals that is directly proportional to σ_0 [45]:

1484
$$au_e = \frac{m}{ne^2} \sigma_0,$$
 (2.184)

 where n is the number density of charge carriers of effective mass m and charge e. The reason for the difference is that τ_e is the average time of travel between *scattering events* (collisions with ions, electrons, phonons or by umklapp), whereas τ_D is the residence time between (effectively instantaneous) *jumps between adjacent sites*. Nor is τ_D equal to τ_E for dielectric relaxation, although they are related by an expression that is derived below.

Equation (2.183) implies that ionic conductivity cannot exceed ca. 10^3 Sm⁻¹, since τ_D cannot reasonably be less than a vibrational lifetime τ_v and ε_∞ is rarely greater than about 10. The vibrational lifetime is conveniently defined by the condition for critical damping (§1.11), $\omega_0 \tau_v = 1$, so that for a typical vibrational frequency of about $f \approx 10^{12}$ Hz $\Rightarrow \omega \approx 6 \times 10^{12}$ rad/s the

value of τ_{v} is about 2×10^{-13} s and

1497
$$\sigma_{0,\text{max}} \approx \frac{e_0 \mathcal{E}_{\infty}}{\tau_V} \approx \frac{\left(8.854 \times 10^{-12} \text{ F/m}\right) (10)}{2 \times 10^{-13} \text{ s}} \approx 450 \text{ S/m},$$
 (2.185)

comparable with the highest conductivity observed for ionic conductors.

The properties of the four basic functions for conductivity relaxation (eq. (2.106)) are conveniently illustrated using a circuit comprising three elements in series: (i) a capacitance $C_s = 10^{-6} \, \text{F} = 1 \, \mu \text{F}$; (ii) a parallel combination of a resistance $R_1 = 10^8 \, \Omega$ and capacitance $C_1 = 10^{-12} \, \text{F} (1 \text{pF})$ (iii) another parallel combination of a resistance $R_2 = 10^6 \, \Omega$ and capacitance $C_1 = 10^{-12} \, \text{F} (1 \text{pF})$. The two parallel R_p - C_p elements could for example simulate crystal and intercrystal impedances in a polycrystalline samples and the series capacitance C_s could simulate electrode polarization. As discussed below this circuit has been used by several groups and will be referred to as the "ideal" conductivity circuit.

The electric modulus $M^* = M' + iM''$ is particularly useful for analyzing conductivity relaxation but it is controversial (a discussion of many of the issues is given in [1]). It was probably first defined by McCrum, Read and Williams [32], but its use in analyzing conductivity relaxation was initiated by Macedo and coworkers [44]. The usefulness of M^* is illustrated by the simplest case of a constant conductivity σ_0 and constant relative permittivity ε_{∞} (the reason for the subscripts will become clear when distribution functions are considered later). Consider the definitions

$$M' = \frac{\varepsilon'}{\varepsilon'^2 + \varepsilon''^2}$$
 (a),

$$M'' = \frac{\varepsilon''}{\varepsilon'^2 + \varepsilon''^2}$$
 (b).

Insertion of the relations $\varepsilon'' = \sigma_0 / e_0 \omega$ and $\varepsilon' = \varepsilon_\infty$ then yields

1520
$$M' = \frac{1}{\varepsilon_{\infty}^{D}} \left(\frac{\omega^2 \tau_D^2}{1 + \omega^2 \tau_D^2} \right) \tag{2.187}$$

1522 and

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$$M'' = \frac{1}{\varepsilon_{\infty}^{D}} \left(\frac{\omega \tau_{D}}{1 + \omega^{2} \tau_{D}^{2}} \right). \tag{2.188}$$

Thus M'' exhibits a desirable peak centered at $\omega_D=1/\tau_D$ as a function of $\ln(\omega)$. The components of the complex resistivity ρ^* are related to those of M^* by (eq. (2.106))

1529
$$\rho' = \frac{M''}{e_0 \omega} = \frac{\tau_D}{e_0 \varepsilon_\infty^D} \left(\frac{1}{1 + \omega^2 \tau_D^2} \right) = \left(\frac{\rho_0}{1 + \omega^2 \tau_D^2} \right)$$
 (2.189)

1531 and

1533
$$\rho'' = \frac{M'}{e_0 \omega} = \frac{\tau_D}{e_0 \varepsilon_{\infty}^D} \left(\frac{\omega \tau_D}{1 + \omega^2 \tau_D^2} \right) = \rho_0 \left(\frac{\omega \tau_D}{1 + \omega^2 \tau_D^2} \right), \tag{2.190}$$

where $\rho_0 = 1/\sigma_0 = \tau_D/e_0 \varepsilon_\infty^D$. The functions M'' and ρ'' have identical frequency dependencies but are weighted by $1/\varepsilon_\infty$ and ρ_0 respectively. The difference in weighting factors can be exploited to considerable advantage in the analysis of ac conductivity data (§2.3.5.6 - §2.3.5.8).

For dielectric relaxation M^* and ε^* are almost equivalent because a Debye peak in ε'' also yields a Debye peak in M'' [44] [see eqs. (2.132) and (2.133)]. The derivation of M^* for a Debye dielectric without any conductivity is given in Appendix 2.1. It might appear that a peak in M'' could be due to either a conductivity or dielectric process and that M^* could not distinguish between them but this is not necessarily so because the average relaxation time $\langle \tau_D \rangle$ will be calculable from the limiting low frequency conductivity [eq. (2.73)] if the process is a conductivity relaxation, and the retardation time will not correlate with σ_0 if the peak in M'' is due to a dielectric relaxation Also $\lim_{\omega \to 0} M'(\omega) = 1/\varepsilon_0$ for dielectric relaxation compared with $\lim_{\omega \to 0} M'_{conductivity}(\omega) = 0$ for conductivity relaxation. The archetypal example of dielectric relaxation being correlated with σ_0 occurs in the alkali silicate glasses and it was this correlation that originally led to the inference that the residual dielectric loss (after subtraction of $\sigma_0/e_0\omega$) is due to the same alkali migration process that produces σ_0 [27-31]. This led Macedo and collaborators [44] to first use M^* in the analysis of conductivity relaxation.

The low frequency conductivity relaxation limit for M ' is revealing because M ' is a measure of the restoring force in response to an electric field perturbation. The low frequency limit of this restoring force is finite for dielectric relaxation because the charge storage ability remains nonzero: $\lim_{\omega \to \infty} \varepsilon'(\omega) = \varepsilon_0$. For conductivity relaxation the dielectric loss becomes infinite as $\omega \to 0$ (dissipation completely overrides any storage capability) and the restoring force is "short circuited". This is precisely analogous to the mechanical modulus going to zero as the viscosity of a viscoelastic material dominates at low frequency and the elasticity disappears. The electric modulus was first introduced to emphasize this mechanical analogy [32].

An alternative to the electric modulus for analyzing materials in which the dielectric loss and conductivity are correlated has been proposed by Johari [46]. This proposal is similar in style to a mechanism for ionic conductivity proposed by Hodge and Angell [47] that was based on the one-dimensional Glarum diffusion model for dielectric relaxation [§1.12.6, Chapter One]. The Glarum model comprises a relaxing dipole that can relax either independently with retardation time τ_0 or by the arrival of a defect of some kind that relaxes it instantly. Hodge and Angell suggested that the dipole is a trapped ion/vacancy pair (known to exhibit Debye dielectric

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behavior, §2.3.1.2) and that the defects are itinerant ions that contribute to σ_0 . Such diffusing ions would eliminate the dipole upon arriving by inserting themselves into the vacancy, consistent with the Glarum model. The average activation energy for oscillation of trapped ions and that for ion migration are presumed to be similar (perhaps identical), thus accounting for the nearly temperature invariant distribution of conductivity relaxation times. The Glarum function is mathematically similar to the Davidson-Cole function that has a (rarely observed) Debye-like low frequency loss. This low frequency behavior arises from the Glarum assumption that the dipole has just one retardation time. However if a distribution of dipole retardation times is assumed, corresponding to a distribution of sites in an amorphous material and/or local fields effects (§2.3.1.2) for example, better agreement with experiment might be obtained without changing the essential physics of the Glarum model.

2.4.2 Distribution of Conductivity Relaxation Times

Both M^* and ρ^* can be formally described in terms of a distribution of conductivity relaxation times:

1582
$$M * (i\omega) = M_{\infty} \int_{-\infty}^{+\infty} g(\ln \tau_D) \left(\frac{i\omega \tau_E}{1 + \omega^2 \tau_D^2} \right) d\ln \tau_D$$
 (2.191)

and similarly for $\rho^*(i\omega)$. A distribution of conductivity relaxation times affects the dispersion of the corresponding complex admittance functions $\varepsilon^*(i\omega)$ and $\sigma^*(i\omega)$:

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$$\sigma_0 = \frac{\mathbf{e}_0 \mathcal{E}_{\infty}^D}{\langle \tau_D \rangle} = \frac{\mathbf{e}_0}{M_{\infty}^D \langle \tau_D \rangle}, \tag{2.192}$$

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$$\sigma_{\infty} = e_0 \varepsilon_{\infty}^D \left\langle \frac{1}{\tau_D} \right\rangle = \frac{e_0}{M_{\infty}^D} \left\langle \frac{1}{\tau_D} \right\rangle,$$
 (2.193)

1590 and

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$$\varepsilon_0^D = \varepsilon_\infty^D \frac{\left\langle \tau_D^2 \right\rangle}{\left\langle \tau_D \right\rangle^2} \ge \varepsilon_\infty^D. \tag{2.194}$$

A distribution of conductivity relaxation times is not easily distinguishable from dielectric and conductivity relaxations occurring together [36,44], although the dielectric relaxation will not be observable if τ_E ? τ_D because σ_0 will then exceed the limiting high frequency dielectric conductivity given by eq. (2.131):

1599
$$\frac{\sigma'(\omega\tau_D \to 0)}{\sigma'_{\mu}(\omega\tau_E \to \infty)} = \frac{\sigma_0}{\sigma_{\mu}(\infty)} = \frac{\varepsilon_{\infty}}{\langle \tau_D \rangle} \left(\frac{\langle \tau_E \rangle}{\varepsilon_0 - \varepsilon_{\infty}}\right) = \frac{\varepsilon_{\infty}}{\varepsilon_0 - \varepsilon_{\infty}} \frac{\langle \tau_E \rangle}{\langle \tau_D \rangle} >> 1.$$
 (2.195)

This phenomenon has been directly observed in systems for which the dielectric retardation time is essentially constant but whose conductivity is increased by addition of electrolyte [48, 49] (also see §2.3.6.9 below).

2.4.3 Constant Phase Element Analysis

It is sometimes useful to have a circuit element for which the phase angle is independent of ω ,

1609
$$W*(i\omega) = W(\omega) \exp\left(\frac{\pm i\alpha\pi}{2}\right),$$
 (2.196)

where $W(\omega)$ is any real function and $0 < \alpha \le 1$ is also real (the positive sign in the exponent corresponds to an admittance and the negative sign to an impedance). However as noted in Chapter One and §2.4.3 eq. (2.196) can only be valid over a restricted frequency range because otherwise the underlying distribution of relaxation/retardation times cannot be normalized. Equation (2.196) is a generalization of the Warburg impedance for which $\alpha = 0.5$.

1617 2.4.4 Estimation of σ_0

Several methods have been published for estimating σ_0 in situations where it has been contaminated by such factors as electrode polarization and intergranular impedances. An accurate value for σ_0 is often important because, in addition to the obvious need for reliable data, its contribution to ε " must be subtracted for permittivity analyses (the attendant difficulties have been discussed by Ravaine and Souquet [52, 53]). Accurate values of σ_0 are also needed in order to determine reliable activation energies for conductivity. For example if $\log(\sigma)$ measured at constant measuring frequency ω_{meas} is plotted against 1/T in the usual Arrhenius fashion then spurious changes in slope can result from both electrode polarization and bulk relaxation effects. (1) If the measuring frequency ω_{meas} is so low that polarization is significant then the measured conductivity will be less than σ_0 , by an amount that increases with increasing temperature because of the shift to higher frequencies of the polarization σ' spectrum (which has essentially the same effective activation energy as the sample conductivity).

(2) A fictitiously low activation energy is then obtained at high temperatures as ω_{meas} probes deeper into the polarization relaxation. A spuriously low activation energy can also occur at low temperatures when ω_{meas} lies within the bulk relaxation frequency range where σ' is often observed to increase as $\omega^{\alpha}(\alpha < 1)$. In this case the measured conductivity will exceed σ_0 by an amount that decreases with increasing temperature and the measured activation energy will be smaller than the true value by the factor $\alpha = d \ln \sigma' / d \ln \omega$:

1637
$$E_{a,obs} = E_{a,true} (1-\alpha)$$
. (2.197)

In cases where $\alpha \approx 1$, as occurs in some electronic semiconductors [48], the fixed frequency conductivity is therefore almost independent of temperature in the bulk relaxation temperature region.

2.4.4.1 Analyses in the Complex Resistivity Plane

Ravaine and Souquet [52,53] used the complex resistivity plane for determining σ_0 of alkali silicate glasses in the presence of electrode polarization using low frequency extrapolations to the real axis. They fitted the high frequency spectrum (i.e. sample relaxation) to the Cole-Cole [54] function (§1.12.5) and extrapolated the Cole-Cole semicircle to the real axis. For severe polarization Armstrong et al. [55-59] used a similar method based on extrapolation of the high frequency polarization spike to the real axis. This method is restricted to high conductivities whose relaxation frequency lies above the measuring frequency range.

2.4.4.2 Modulus and Resistivity Spectra

In cases where electrode polarization and conductivity relaxations overlap significantly and no plateau in σ' is observed, σ_0 can be estimated from eq. (2.183) if $\langle \tau_D \rangle$ and ε_{∞} are known.

These can sometimes be determined with sufficient precision by fitting $M''(\omega)$ to an appropriate empirical function because M'' is insensitive to high capacitance effects such as electrode polarization and intergranular impedances so that only the bulk relaxation is included in the fitted function. For this application the fit to M'' should preferably be weighted by the lower frequency data because these reflect the longer relaxation time components of the distribution that contribute more significantly to $\langle \tau_D \rangle$. The maximum in ρ'' , ρ_{\max} , can also be used to estimate σ_0 to within about 10% if the full width at half height of the peak in ρ'' (Δ decades) can be determined:

1663
$$\sigma_0 \approx \frac{1}{1.75 \Delta \rho_{\text{max}}}$$
 (2.198)

If only the maximum in ρ " at ω_{max} is observable σ_0 can still be estimated from the value of ρ ' at ω_{max} by assuming ρ " (ln ω) to be symmetric:

$$1668 \qquad \sigma_0 \approx \frac{1}{2\rho'(\omega_{\text{max}})}. \tag{2.199}$$

2.4.4.3 Complex Admittance Plane

One of the first applications of complex plane plots was to polycrystalline yttria-zirconia electrolytes by Bauerle [60]. Bauerle gave an excellent discussion of equivalent circuits and their corresponding complex admittance plane plots, but the only circuit used in their data analysis was

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a series combination of two parallel R_pC_p elements and a series resistance R_s . The first parallel R_pC_p element in this circuit represented the electrode interface: the capacitance of a double layer in parallel with the resistance of an oxygen gas-oxide ion charge transfer process. The second R_pC_p element represented an intergranular boundary ("constriction") impedance, and the pure resistance simulated the bulk crystal. The experimentally observed complex admittance plane plots were in excellent agreement with the equivalent circuit predictions. The zero frequency conductivity predicted from the complex plane plot was also in excellent agreement with four terminal data, and the expected dependence of the electrode impedance on oxygen partial pressure was observed. Despite these successes, some disadvantages of the method should be pointed out. First, in assuming that the bulk crystal acts as a pure resistance the analysis implicitly assumes that the measuring frequencies are well below the conductivity relaxation frequency, that can only be confirmed retrospectively. Second, although there are three relaxing elements (since the sample resistance must realistically have a capacitance in parallel with it), the complex admittance plane exhibits only two arcs that reflect the differences between the relaxing elements. If the observed relaxations overlap significantly, an assumption must be made about the shapes of the two relaxations before extrapolations are made, i.e. a functional form for the extrapolating function must be chosen. Bauerle's data were well described by the Cole-Cole function but this would not be expected to occur in general.

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2.4.5 Examples

2.4.5.1 Electrode Polarization and Bulk Relaxation in the Frequency Domain

Consider an "ideal" equivalent circuit similar to that used by Bauerle except that the series resistance is replaced by a series capacitance, with specific values of the parallel R_pC_p elements being $\left[R_1=10^8\,\Omega,C_1=10^{-11}\mathrm{F}\Rightarrow\tau_1=R_1C_1=10^{-3}\,\mathrm{s}\right], \left[R_2=10^6\,\Omega,C_2=10^{-11}\mathrm{F}\Rightarrow\tau_2=R_2C_2=10^5\,\mathrm{s}\right]$ and $\left[C_s=10^{-6}\,\mathrm{F}\right]$. The distribution of conductivity relaxation times then comprises two delta functions at $\tau_1=10^{-3}\,\mathrm{s}$ and $\tau_2=10^{-5}\,\mathrm{s}$. The shorter relaxation time element simulates the crystal

impedance in a polycrystalline preparation, the longer relaxation time element simulates an intergranular impedance, and the series capacitance simulates electrode polarization. This circuit has been found to be useful in analyzing the electric response of a variety of conducting materials, including a superionic conductor [61], an electronic semiconductor [62], and a normal ionic

1704 conductor [9]. The relaxation time averages are

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1706
$$\left\langle \tau_D^2 \right\rangle = \frac{\tau_1^2 + \tau_2^2}{2} = 5.0005 \times 10^{-9} \text{ s}$$
 (2.200)

1707
$$\langle \tau_D \rangle = \frac{\tau_1 + \tau_2}{2} = 5.05 \times 10^{-5} \text{ s}$$
 (2.201)

1708
$$\left\langle \tau_D^{-1} \right\rangle = \frac{\tau_1^{-1} + \tau_2^{-1}}{2} = 5.05 \times 10^{+5} \text{ s}$$
 (2.202)

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The high frequency relative permittivity is (assuming k=1 for convenience so that $C_0 = \mathbf{e}_0$ numerically)

1713
$$\varepsilon_{\infty} = \frac{C_1 C_2}{e_0 (C_1 + C_2)} = 5.647,$$
 (2.203)

1715 and the low frequency relative permittivity is

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$$\varepsilon_0 = \varepsilon_\infty \frac{\left\langle \tau_D^2 \right\rangle}{\left\langle \tau_D \right\rangle^2} = \left(5.647\right) \frac{\left(5.005 \times 10^{-9}\right)}{\left(5.05 \times 10^{-5}\right)^2} = 11.083. \tag{2.204}$$

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1719 The limiting low and high frequency conductivities are

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$$\sigma_0 = \frac{\epsilon_0 \varepsilon_\infty}{\langle \tau_D \rangle} = \frac{\left(8.854 \times 10^{-12}\right) \left(5.647\right)}{\left(5.05 \times 10^{-5}\right)} = 9.9 \times 10^{-7} \,\mathrm{S m^{-1}}$$
 (2.205)

1722
$$\sigma_{\infty} = \epsilon_0 \varepsilon_{\infty} \langle 1/\tau_D \rangle = (8.854 \times 10^{-12}) (5.647) (5.05 \times 10^{+5}) = 2.53 \times 10^{-5} \text{ S m}^{-1}.$$
 (2.206)

1723

- 1724 The ρ " and M" spectra both exhibit two peaks the heights of which reflect the different 1725 weighting of the two functions - eqs. (2.188) and (2.190). The two ρ " peak heights differ by the ratio of the resistances $10^8/10^6 = 10^2$, whereas the M" peaks are equal in height because the two 1726 1727 capacitances are equal. If the capacitances were different and the resistances the same then the peaks in ρ " would have the same height and those in M" would differ. Also ρ " increases 1728 indefinitely at low frequencies due to C_s whereas M'' is unaffected. 1729
- After subtraction of the contribution of σ_0 to ε ", and of the limiting high frequency 1730 contribution of $\varepsilon_{\scriptscriptstyle \infty}$ to σ ", both σ " and ε " exhibit a single peak at a frequency between the two
- 1732 maxima exhibited in the M" and ρ " spectra. These single peaks in the admittance functions occur
- 1733 because at intermediate frequencies the high frequency RC element behaves as a resistance and
- 1734 the low frequency RC element behaves as a capacitance. As noted in §2.2.4 the effectively series
- RC circuit will produce just a single loss peak in the admittance. For the electrode polarization 1735 relaxation caused by C_s in series with the sample resistance $(R_1 + R_2)$ peaks in $\sigma'' - e_0 \varepsilon_\infty \omega$ and 1736
- ε "- σ_0 / $e_0\omega$ are observed at lower frequencies. 1737
- A low frequency decrease in σ' and increases in ε' and ρ'' are found that are due to the 1738 electrode polarization simulated by C_s . For expositional clarity the value of C_s was chosen to 1739
- 1740 ensure a clean separation between the simulated polarization and bulk relaxations but this does
- not occur in typical experimental data. 1741
- 1742 The complex plane plots have both advantages and disadvantages compared with the
- spectra. Two disadvantages are the inconvenience of locating the frequencies of maximum loss, 1743
- and of comparing these frequencies in M^* and ρ^* plots because of the opposite directions of 1744
- increasing frequency. On the other hand, complex plane plots are useful for extrapolations. For 1745
- example in highly conducting materials whose conductivity relaxation frequency $1/\langle \tau_D \rangle$ lies 1746
- 1747 above the measuring frequency, and for which electrode polarization is significant or even severe,

the polarization spike in the ρ^* plane can be extrapolated to the real axis to give an estimate of $\sigma_0 = 1/\rho_0$. At frequencies above the conductivity relaxation frequency, σ_0 is manifested as a spike in the ε^* plane, corresponding to the limiting values of $\lim_{\omega \to 0} \varepsilon'' = \lim_{\omega \to 0} \sigma_0 / \epsilon_0 \omega = \infty$ and $\lim_{\omega \to 0} \varepsilon'' = \varepsilon_0$.

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2.4.5.2 Conductivity Relaxation in Sodium β – Alumina

Permittivity, modulus and resistivity spectra of single crystal sodium β -alumina at 113 K have been reported by Grant and Ingram [64,65]:

- (i) the ε " spectrum measured in the direction perpendicular to the conduction planes;
- (ii) the M'' spectra in orientations perpendicular and parallel to the conducting planes;
- (iii) the Z" spectrum measured in the direction of the conduction planes.

The frequency of maximum Z" in the parallel orientation was close to the frequency of maxima in M" and ε " measured in the perpendicular orientation, and the activation energy for the parallel resistivity spectrum was close to that for the perpendicular dielectric loss spectrum. The data for the perpendicular orientation were interpreted in terms of a Maxwell layered dielectric [65], with each insulating spinel block being a capacitance and each conduction plane a resistance. The activation energy for the dielectric loss was thus determined by that of the conductivity of the conducting layers, that the data suggest is similar in directions parallel and perpendicular to the conduction planes. An extraordinarily large width of the M'' spectrum for single crystal Na β – alumina was observed in the parallel orientation [66,67], indicating a very broad distribution of conductivity relaxation times: the resistivity and modulus spectra taken together suggested that the distribution was bimodal. Grant and Ingram proposed that at 113 K the low frequency conductivity is determined by an activated localized ion motion that is the same in both orientations. The higher frequency conductivity, which contributed to M'' but not to ρ'' , resulted from a relatively free motion of ions crossing low energy barriers. These processes were consistent with low temperature localization of sodium ions deduced from NMR data [68]. Localized activation is not the rate determining step at high temperatures and the well-established low activation energy for conductivity in sodium β -alumina was observed. Spectra of M'' and Z''for a representative polycrystalline specimen at 113 K were also reorted. The Z" spectrum was uninformative at this temperature, increasing monotonically at low frequencies due to electrode polarization. The M" spectrum exhibited a maximum at about the same frequency as the single crystal M" spectrum observed perpendicular to the conduction planes, and a reproducible shoulder was observed at about the same frequency as M'' observed parallel to the conduction planes in single crystals.

This work demonstrates that comparison of the functions M'', ρ'' and ε'' can uncover details of the conductivity behavior of sodium β -alumina that could not even be discussed if only σ^* and ε^* data were used.

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2.4.5.3 Complex Impedance Plane Analysis of Electrode Polarization in Sintered β – Alumina.

The use of the complex impedance plane for extrapolating polarization phenomena to

obtain data on the bulk material was used extensively by Armstrong and coworkers in their studies of superionic conductors such as Na β -alumina [55] and Ag-Rb iodide [54-58]. A spike in the complex impedance plane corresponds to the low frequency increase in Z'' due to the series electrode capacitance and extrapolation of this spike to the real axis yielded the limiting low frequency values of Z' and therefore of ρ_0 . Different surface preparations were observed to affect the measured impedance but all of the extrapolations gave the same values for ρ_0 . This method is clearly most appropriate for very highly conducting materials whose conductivity relaxation lies at frequencies well above those used experimentally.

> 2.4.5.4 Complex Impedance Plane Analysis of Atmosphere Dependent Electrode Effects in KHF₂ Complex impedance plane analysis was also used by Bruinink and Broers [69] for the α and β phases of KHF₂. In an atmosphere of hydrogen with platinum paint electrodes, the complex impedance plane plot of data for α -KHF₂ was consistent with a Warburg impedance in parallel with the bulk resistance and capacitance [69], and extrapolation to the real axis gave a value of ρ_0 in agreement with a separately determined four terminal dc value. This plot gave no indication of interfacial polarization, consistent with α -KHF₂ being a proton conductor and the platinum paint electrodes behaving as reversible hydrogen electrodes. This contrasted sharply with the low frequency behavior of α -KHF₂ in a vacuum, where a double layer capacitance of about 440 mF m⁻² per electrode in parallel with a Faradaic resistance of about $2\times10^4\Omega$ m per electrode produced an additional semicircle in the complex plane. For the polycrystalline β -phase the complex plane plot was essentially unchanged for data taken in both a hydrogen atmosphere and a vacuum [69] and is consistent with a Warburg impedance in series with a parallel RC element, corresponding to electrode polarization due to blocking of K⁺ and/or F⁻ charge carriers. An RC transmission line was used to rationalize the Warburg impedance in terms of bulk electrical relaxation.

2.4.5.5 Intergranular Effects in Polycrystalline Electrolytes

The effects of intergranular material on the overall electrical response of polycrystalline electrolytes have been extensively documented. Only one example is discussed here [9,66]. The simplest equivalent circuit representation of such materials comprises two parallel RC elements in series, where one element is associated with a crystallite and the other with intergranular material. Armstrong et al. [70] showed that such a series circuit can represent the principle features of polycrystalline electrolytes. Since the interface is thin and the permittivities of ionic solids typically vary by a factor of less than 10, the capacitance C_i associated with the interface is much higher than that of the grain C_p :

$$C_{i} = \frac{\epsilon_{0} \varepsilon' A_{i}}{d_{i}} >> \epsilon_{0} \varepsilon' = k C_{p}$$

$$(2.207)$$

where A_i is the average cross section area, d_i is the average thickness of the intergranular material, and $k = e_0 / C_0$ is the cell constant.

1831 2.4.5.6 Intergranular Cracking

Experimental M'' and ρ'' spectra for a polycrystalline material known to have intergranular cracking were reported in [9]. The spectra were similar to those for two parallel R_pC_p elements in series although the experimental peaks were broader - they could be approximated as the sum of two Debye peaks of equal heights separated by about a decade in frequency, so that the maxima in Z'' and M'' could be approximated as $R_p/4$ and $C_0/4C_p$, respectively. Computed values of R and C for the intergranular and granular material in the cracked sample, using these approximations and assuming a resolution into symmetric ρ'' peaks, were:

1839 were

1841 Lower Frequency (Intergranular) Relaxation in Cracked Sample

1842
$$\tau_i = \frac{1}{\omega_{\max(Z'')}} = 6.4 \times 10^{-6} \text{ s},$$
 (2.208)

1843
$$R_i \approx 4Z_{\text{max}}^{"} = 6.4 \times 10^6 \,\Omega,$$
 (2.209)

1844
$$C_i = \frac{\tau_i}{R_i} \approx 1.0 \,\mathrm{pF}$$
. (2.210)

1846 Higher frequency (Intragranular) Relaxation in Cracked Sample

1847
$$au_c = \frac{1}{\omega_{\max(Z'')}} = 1.6 \times 10^{-7} \text{ s}, ag{2.211}$$

1848
$$R_c \approx 4Z_{\text{max}}^{"} = 2.6 \times 10^6 \,\Omega,$$
 (2.212)

1849
$$C_c = \frac{\tau_c}{R_c} \approx 0.06 \,\mathrm{pF}$$
 (2.213)

The impedance spectrum was drastically altered after the intergranular cracking had been annealed out [9]. A single peak in Z'' was observed in the annealed sample that was essentially indistinguishable from the high frequency peak in the cracked material, strongly suggesting that it was due to intra-crystal relaxation and that the additional low frequency peak for the cracked sample was due to thin air gaps. Consistent with this, the modulus spectrum was essentially unchanged by annealing since it was unaffected by the high capacitance cracks. The estimates of the intragranular and intergranular resistances were confirmed by the σ_0 data: the observed conductivity of the cracked sample was largely determined by the intergranular resistance, and the ratio of the conductivities of the sample before and after annealing should have been

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$$\frac{Z_{\max}^{\text{nlow}\omega} + Z_{\max}^{\text{nligh}\omega}}{Z_{\max}^{\text{nligh}\omega}} = \frac{2.25 \times 10^6}{0.65 \times 10^6} = 3.5,$$
 (2.214)

in fair agreement with

$$\frac{\sigma_{annealed}}{\sigma_{cracked}} = 3.1. \tag{2.215}$$

The combination of modulus and impedance spectroscopies once again revealed details that could not be obtained from the original σ' and ε' data.

2.4.5.7 Intergranular Gas Adsorption

The effects of oxygen and alkali doping on the electrical response of polycrystalline zinc oxide were studied by Seitz and Sokoly [71]. Only the effects of oxygen pressure are discussed here. An increase in conductivity was observed with decreasing oxygen pressure and the absence of changes due to different electrode materials implied that adsorbed oxygen at grain surfaces was responsible for the observed polarization of the sample. The conductivity and permittivity were plotted explicitly as a function of frequency and these data allowed M'' and ρ'' spectra to be calculated without difficulty (unpublished results obtained by the present author). The calculated M'' and ρ'' spectra exhibited two partially resolved peaks whose estimated magnitudes were consistent with a thin high capacitance - high resistance layer determining the low frequency response. Both peaks in the M'' spectrum had comparable half widths (ca. 1.5 decades) and their relative maximum values 8×10^{-4} and 1.1×10^{-2} (ratio 14) were a good (inverse) measure of the relative capacitance of each relaxation: $C_1/C_h\approx13$. The resistance ratio R_1/R_h of the low frequency high frequency relaxation could then be estimated from the two values of $f_{\rm max}$ (ca. 5×10^2 and 3×10^5 Hz) to be about 45:

$$\frac{R_1 C_1}{R_h C_h} \approx 600 \approx \frac{13 R_1}{R_h} \Longrightarrow \frac{R_1}{R_h} \approx 45. \tag{2.216}$$

The conductivity estimated from the height of the lower frequency resistivity peak was 1.1×10^{-7} S m⁻¹, in reasonable agreement with the low frequency plateau value of 1.3×10^{-7} S/m. From the relative frequencies of the M'' maxima and the relative heights of the (partly resolved) ρ'' maxima, the conductivity of the high frequency relaxation was estimated to be about $10^{-6\pm1}$ S m⁻¹. Because of its higher associated capacitance the lower frequency relaxation almost certainly corresponded to an intergranular impedance, and its removal by a reduction in oxygen pressure should therefore have increased the sample conductivity by about 45 but have a small effect on the measured permittivity (since removal of a high series capacitance has little effect on the total impedance). This predicted change in resistivity agreed with the qualitative statement that conductivity increased with decreasing oxygen pressure [71].

1900 Appendices

1901

1902 Appendix 2.1 Derivation of M^* for a Debye Relaxation with No Additional Separate Conductivity

These derivations are shown for pedagogical clarity rather than mathematical elegance.

1905 (1)
$$\Delta \varepsilon \equiv \varepsilon_0^E - \varepsilon_\infty^E; \tau_D = \left(\varepsilon_\infty^E / \varepsilon_0^E\right) \tau_E; M_0^E = 1/\varepsilon_0^E; M_\infty^E = 1/\varepsilon_\infty^E$$

1906 (2)
$$M^* = 1/\varepsilon^* \Rightarrow M' = \frac{\varepsilon'}{\varepsilon'^2 + \varepsilon''^2}; M'' = \frac{-\varepsilon''}{\varepsilon'^2 + \varepsilon''^2}$$

1907 (3)
$$\varepsilon' = \varepsilon_{\infty}^{E} + \frac{\left(\varepsilon_{0}^{E} - \varepsilon_{\infty}^{E}\right)}{1 + \omega^{2} \tau_{E}^{2}} = \varepsilon_{\infty}^{E} + \frac{\Delta \varepsilon}{1 + \omega^{2} \tau_{E}^{2}}; \varepsilon'' = \frac{\Delta \varepsilon \omega \tau_{E}}{1 + \omega^{2} \tau_{E}^{2}}$$

$$\varepsilon'^{2} + \varepsilon''^{2} = \left(\varepsilon_{\infty}^{E}\right)^{2} + \frac{2\varepsilon_{\infty}^{E} \Delta \varepsilon}{1 + \omega^{2} \tau_{E}^{2}} + \frac{\Delta \varepsilon^{2}}{\left(1 + \omega^{2} \tau_{E}^{2}\right)^{2}} + \frac{\Delta \varepsilon^{2} \omega^{2} \tau_{E}^{2}}{\left(1 + \omega^{2} \tau_{E}^{2}\right)^{2}}$$

$$= \frac{\left(\varepsilon_{\infty}^{E}\right)^{2} \left(1 + \omega^{2} \tau_{E}^{2}\right) + 2\varepsilon_{\infty}^{E} \Delta \varepsilon + \Delta \varepsilon^{2}}{1 + \omega^{2} \tau^{2}} = \frac{\left(\varepsilon_{0}^{E}\right)^{2} + \left(\varepsilon_{\infty}^{E}\right)^{2} \omega^{2} \tau_{E}^{2}}{1 + \omega^{2} \tau^{2}}$$

$$M' = \left(\frac{\varepsilon_{\infty}^{E}\left(1 + \omega^{2}\tau_{E}^{2}\right) + \Delta\varepsilon}{1 + \omega^{2}\tau_{E}^{2}}\right) \left(\frac{1 + \omega^{2}\tau_{E}^{2}}{\left(\varepsilon_{0}^{E}\right)^{2} + \left(\varepsilon_{\infty}^{E}\right)^{2}\omega^{2}\tau_{E}^{2}}\right) = \left(\frac{\varepsilon_{0}^{E} + \varepsilon_{\infty}^{E}\omega^{2}\tau_{E}^{2}}{\left(\varepsilon_{0}^{E}\right)^{2} + \left(\varepsilon_{\infty}^{E}\right)^{2}\omega^{2}\tau_{E}^{2}}\right) = \left[\frac{\varepsilon_{0}^{E} + \varepsilon_{\infty}^{E}\omega^{2}\tau_{E}^{2}}{\left(\varepsilon_{0}^{E}\right)^{2} + \left(\varepsilon_{\infty}^{E}\right)^{2}\omega^{2}\tau_{E}^{2}}\right) = \left[\frac{\varepsilon_{0}^{E} + \varepsilon_{\infty}^{E}\omega^{2}\tau_{E}^{2}}{\left(\varepsilon_{0}^{E}\right)^{2} + \left(\varepsilon_{\infty}^{E}\right)^{2}\omega^{2}\tau_{E}^{2}}\right]$$

1909 (4)
$$= \frac{1}{\varepsilon_{0}^{E}} + \frac{\varepsilon_{\infty}^{E}\omega^{2}\tau_{E}^{2} - \frac{\varepsilon_{\infty}^{2}}{\varepsilon_{0}}\omega^{2}\tau_{E}^{2}}{\left(\varepsilon_{0}^{E}\right)^{2}} = \frac{1}{\varepsilon_{0}^{E}} + \frac{\frac{\varepsilon_{\infty}^{E}}{\left(\varepsilon_{0}^{E}\right)^{2}}\omega^{2}\tau_{E}^{2}}{\left(\varepsilon_{0}^{E}\right)^{2}} = \frac{1}{\varepsilon_{0}^{E}} + \frac{\frac{\varepsilon_{\infty}^{E}}{\left(\varepsilon_{0}^{E}\right)^{2}}\omega^{2}\tau_{E}^{2}}{\left(1 + \frac{\left(\varepsilon_{\infty}^{E}\right)^{2}}{\left(\varepsilon_{0}^{E}\right)^{2}}\omega^{2}\tau_{E}^{2}\right)} = \frac{1}{\varepsilon_{0}^{E}} + \frac{\frac{\varepsilon_{\infty}^{E}}{\left(\varepsilon_{0}^{E}\right)^{2}}\omega^{2}\tau_{E}^{2}}{\left(1 + \frac{\left(\varepsilon_{\infty}^{E}\right)^{2}}{\left(\varepsilon_{0}^{E}\right)^{2}}\omega^{2}\tau_{E}^{2}\right)} = \frac{1}{\varepsilon_{0}^{E}} + \frac{\left(\frac{1}{\varepsilon_{\infty}^{E}} - \frac{1}{\varepsilon_{0}^{E}}\right)\left(\varepsilon_{\infty}^{E}\right)^{2}\omega^{2}\tau_{E}^{2}}{\left(1 + \omega^{2}\tau_{D}^{2}\right)} = M_{0}^{E} + \frac{\left(M_{\infty}^{E} - M_{0}^{E}\right)\omega^{2}\tau_{D}^{2}}{\left(1 + \omega^{2}\tau_{D}^{2}\right)} = M_{0}^{E} + \frac{\left(M_{\infty}^{E} - M_{0}^{E}\right)\omega^{2}\tau_{D}^{2}}{\left(1 + \omega^{2}\tau_{D}^{2}\right)}$$

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1915

$$M'' = \left(\frac{-\Delta \varepsilon \omega \tau_{E}^{2}}{1 + \omega^{2} \tau_{E}^{2}}\right) \left(\frac{1 + \omega \tau_{E}^{2}}{\left(\varepsilon_{0}^{E}\right)^{2} + \left(\varepsilon_{\infty}^{E}\right)^{2} \omega^{2} \tau_{E}^{2}}\right) = \left(\frac{-\Delta \varepsilon \omega \tau_{E}}{\left(\varepsilon_{0}^{E}\right)^{2} \left(1 + \frac{\left(\varepsilon_{\infty}^{E}\right)^{2}}{\left(\varepsilon_{0}^{E}\right)^{2}} \omega^{2} \tau_{E}^{2}\right)}\right)$$

1911 (5)
$$= \left(\frac{-\Delta \varepsilon \frac{1}{\varepsilon_{0} \varepsilon_{\infty}^{E}} \frac{\varepsilon_{\infty}^{E}}{\varepsilon_{0}^{E}} \omega \tau_{E}}{\left(1 + \frac{\left(\varepsilon_{\infty}^{E}\right)^{2}}{\left(\varepsilon_{0}^{E}\right)^{2}} \omega^{2} \tau_{E}^{2}\right)} \right) = \frac{\left(M_{\infty}^{E} - M_{0}^{E}\right) \omega \tau_{D}}{\left(1 + \omega^{2} \tau_{D}^{2}\right)}$$

1912
1913 A Matlab®/Octave program for computing the components of *M** with added conductivity is given below in Appendix 2.2.

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```
1916
1917
        Appendix 2.2 Matlab®/GNU Octave Codes
1918
        Computation Code for a Debye Relaxation with Additional Separate Conductivity \sigma_0.
1919
               The algebraic derivation is excessively tedious and is replaced here by a
1920
        Matlab®/GNUOctave code that plots both components of the \varepsilon^* and M^* functions. The values
1921
        of the input parameters are entered by editing the m-file.
1922
1923
        % FUNCTION DebyeCondM Computes and Plots M* for Debye E* plus constant conductivity
1924
        function HD = DebyeCondM
1925
        w = logspace(-6, +6, 1200);
1926
        Logw = log10(w);
1927
        E00 = 8.854E-12;
                                    % Vacuum permittivity in F/m
1928
        E0D = 20;
                                    % Low f dielectric relative permittivity
1929
        EinfD = 10;
                                    % High f dielectric relative permittivity
1930
        DelE = E0D - EinfD;
                                    % Dielectric dispersion range
1931
        EinfE = 3;
                                    % High f conductivity relative permittivity
1932
        TauD = 10^{-4}
                                    % Dielectric relaxation time
1933
        Sigma0 = 10^{-15};
                                    % Conductivity in S/m
1934
        Tausig = E00*EinfE/Sigma0 % Conductivity relaxation time
1935
        E2sig = Sigma0./(E00*w);
                                    % Conductivity contribution to E2
1936
        % CALCULATE E1 and E2
1937
        wTauD = w*TauD:
1938
        Num = 1./(1 + wTauD.^2);
1939
        E1 = EinfD + DelE*Num;
                                    %Debye E1
1940
        E2 = DelE*wTauD.*Num + E2sig; % Debye E2 + Conductivity E2
1941
        Denom = E1.^2 + E2.^2;
1942
        M1 = E1./Denom;
1943
        M2 = E2./Denom;
1944
        subplot (2,2,1);
1945
        plot (Logw, E1);
1946
        ylabel("E1");
1947
        subplot (2,2,2);
1948
        plot (Logw, E2);
1949
        ylabel("E2");
1950
        subplot (2,2,3);
1951
        plot (Logw, M1);
1952
        ylabel("M1");
1953
        subplot (2,2,4);
1954
        plot (Logw, M2);
1955
        ylabel("M2");
1956
1957
        return
1958
```

1960 Appendix 2.3 Derivation of Debye Dielectric Expression from Equivalent Circuit

1961 Impedance of $R_s + C_s$ is

1962
$$Z_s = R_s + 1/i\omega C_s = (1 + i\omega R_s C_s)/i\omega C_s = (1 + i\omega \tau_s)/i\omega C_s$$
 (C1)

1963 and its admittance is

$$1964 A_s = 1/Z_s = i\omega C_s / (1 + i\omega \tau_s) (C2)$$

1965 where $\tau_s \equiv R_s C_s$. The total admittance is

1966
$$A^* = i\omega C_s / (1 + i\omega \tau_s) + G_p + 1 / (i\omega C_p)$$
 (C3)

and the complex capacitance is

$$C^* = A^*/i\omega = C_n + C_s/(1+i\omega\tau_s) + G_n/i\omega$$

$$=\frac{C_{p}\left(1+i\omega\tau_{s}\right)+C_{s}}{1+i\omega\tau_{s}}+\frac{G_{p}}{i\omega}=\frac{\left[C_{p}\left(1+i\omega\tau_{s}\right)+C_{s}\right]\left(1-i\omega\tau_{s}\right)}{1+\omega^{2}\tau_{s}^{2}}+\frac{G_{p}}{i\omega}$$

$$\frac{\left[C_{p}\left(1+\omega^{2}\tau_{s}^{2}\right)+C_{s}\left(1-i\omega\tau_{s}\right)\right]}{1+\omega^{2}\tau_{s}^{2}}-\frac{iG_{p}}{\omega}$$

$$=\frac{\left[C_{p}\left(1+\omega^{2}\tau_{s}^{2}\right)+C_{s}\right]}{1+\omega^{2}\tau_{s}^{2}}-\frac{i\omega\tau_{s}C_{s}}{1+\omega^{2}\tau_{s}^{2}}-\frac{iG_{p}}{\omega}$$
(C4)

1969 from which eqs. (2.154) and (2.155) obtain

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